



CDS 101/110: Lecture 3.1

Linear Systems

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Gates-Thomas 245

Goals for Today:

- Describe and motivate linear system models:
- Summarize properties, examples, and tools
 - Convolution equation describing solution in response to an input
 - Step response, impulse response
 - Frequency response
- Characterize stability and performance of linear systems in terms of eigenvalues

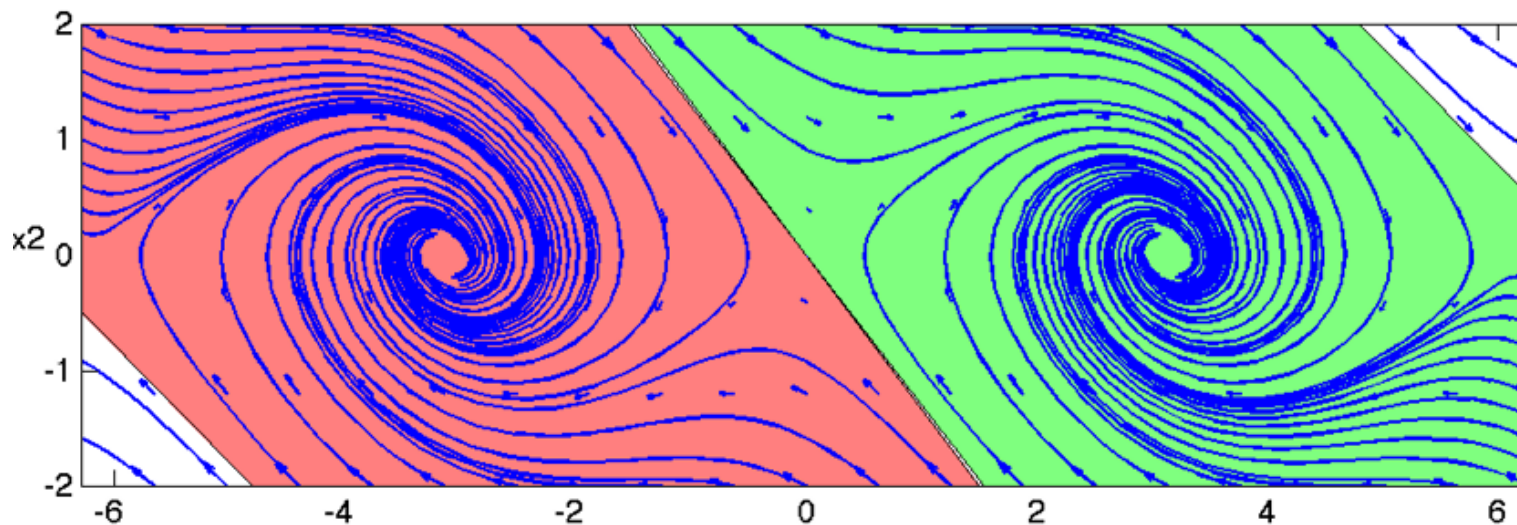
Reading:

- Åström and Murray, Analysis and Design of Feedback Systems, Ch 5

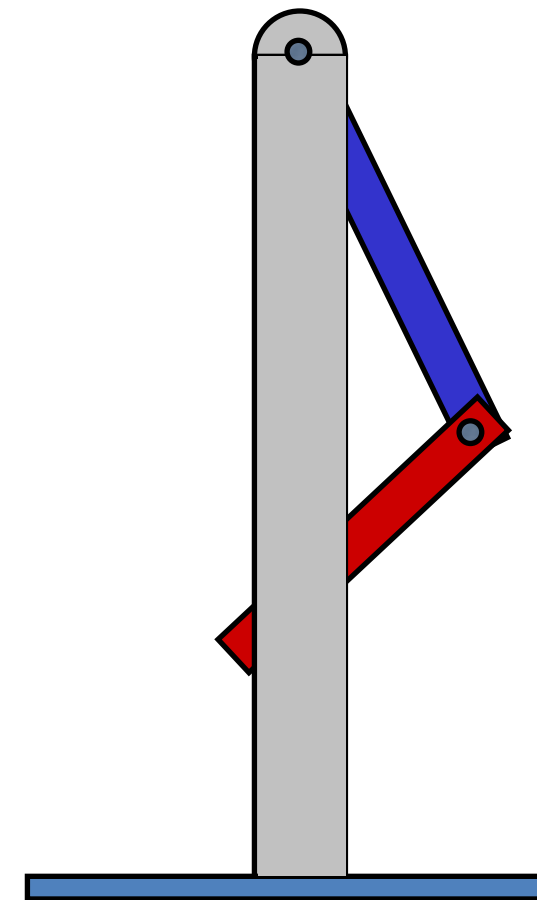
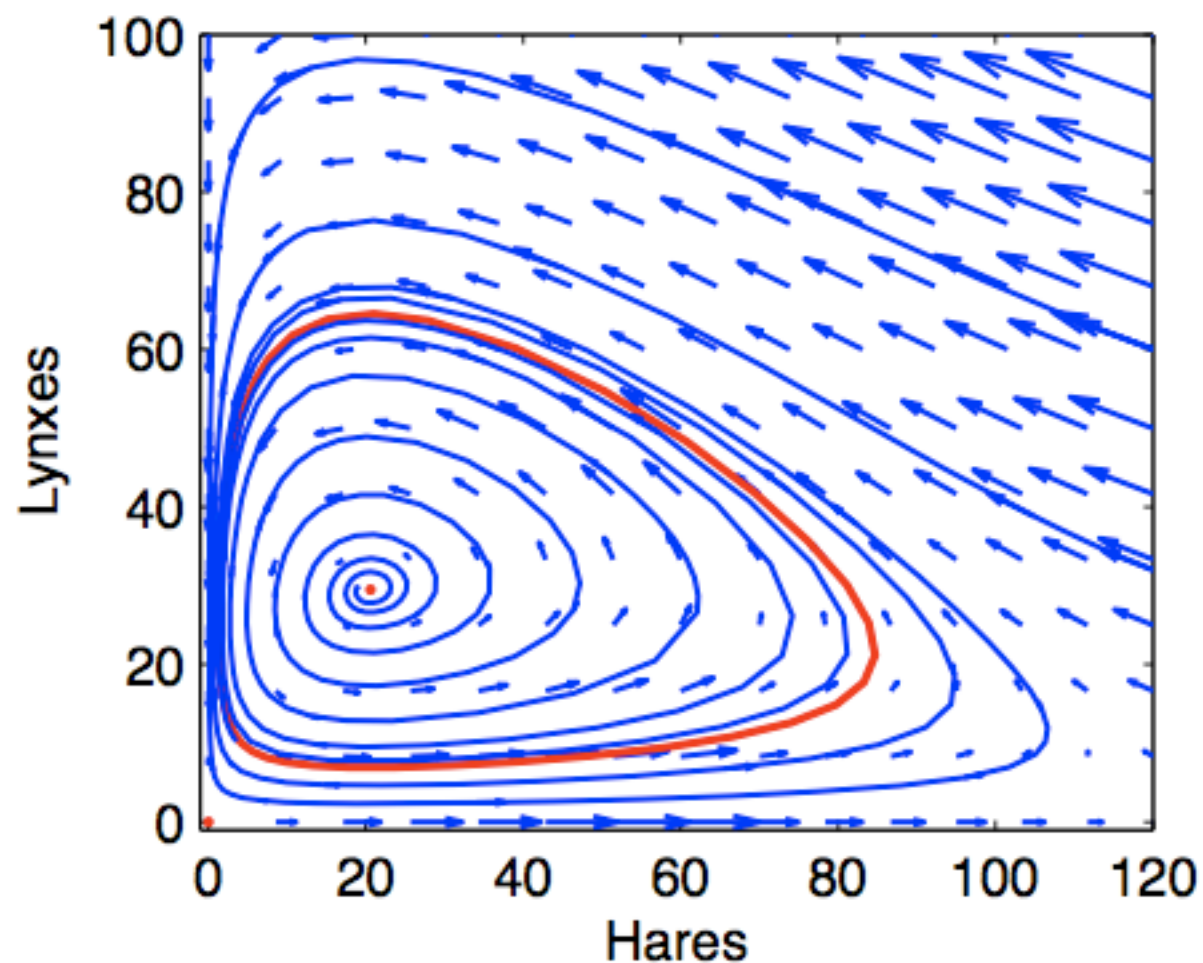
Homework: On course website Monday night



Quick Review: Stability and Performance



- Key topics
 - Stability of equilibrium points
 - Eigenvalues determine stability for linear systems
 - Local versus global behavior



CDS 140, 240 goes into much more detail



Linear Systems

Recall: Linearity of Functions $f: \mathbb{R}^n \rightarrow \mathbb{R}^n$

- Addition: $f(x + y) = f(x) + f(y)$
 - Scaling: $f(\alpha x) = \alpha f(x)$
 - Zero at the Origin: $f(0) = 0$
- } $f(\alpha x + \beta y) = \alpha f(x) + \beta f(y)$

Linear System: $S: u(t) \rightarrow x(t)$

- If $S: u_1(t) \rightarrow x_1(t); \quad S: u_2(t) \rightarrow x_2(t)$
 - $\alpha x_1(t) + \beta x_2(t) = S\{\alpha u_1(t) + \beta u_2(t)\}$

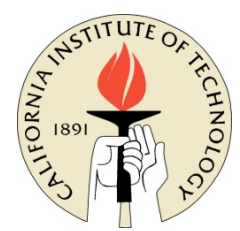
Linear Control System:

- $\dot{x}(t) = A x(t) + B u(t)$
- $y(t) = C x(t) + D u(t)$

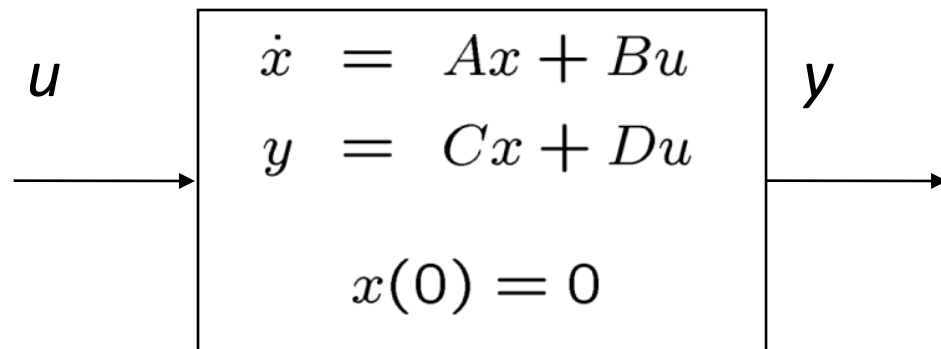
$x(t)$ is system “state”;

$u(t)$ are control inputs

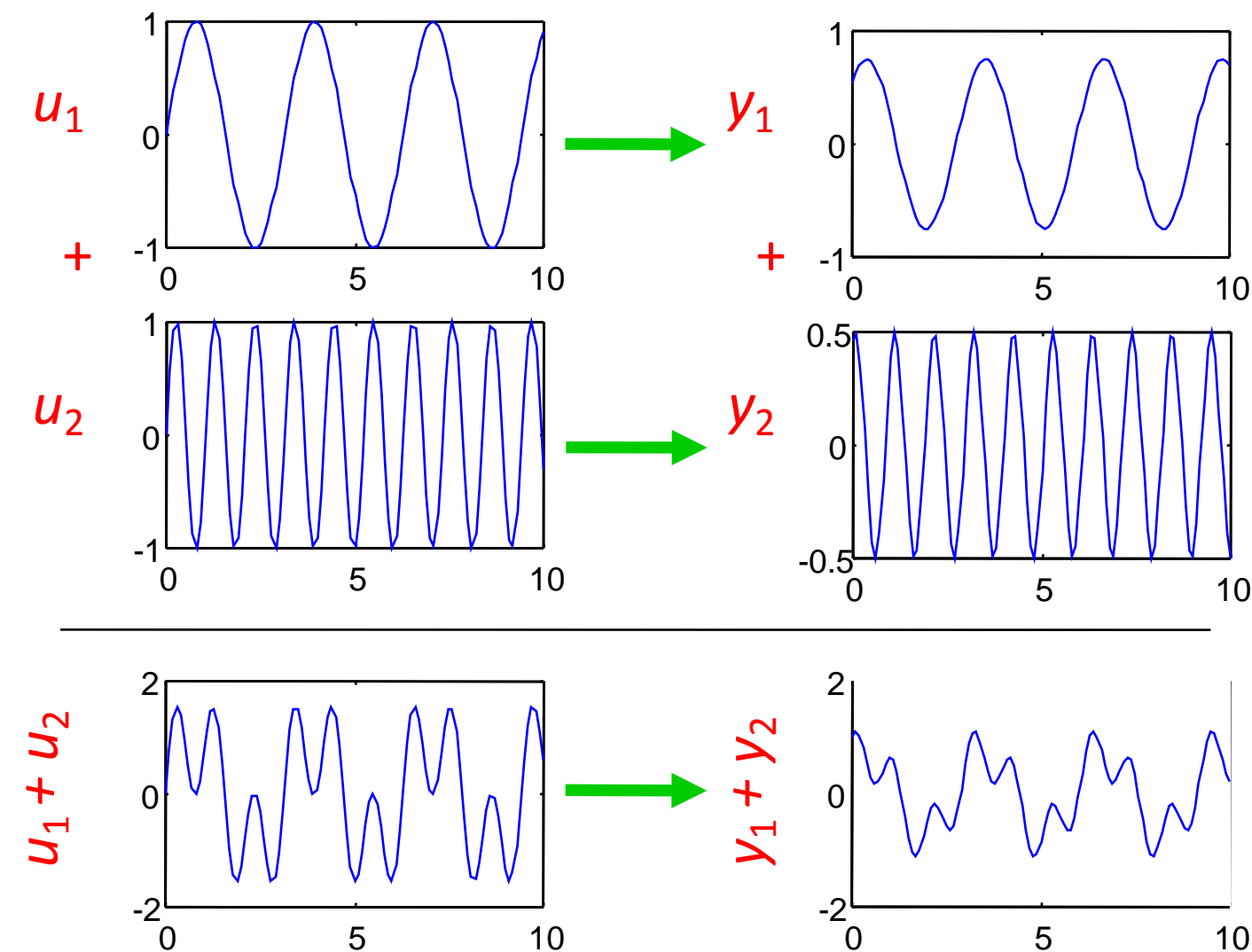
$y(t)$ is the system output,
(what is observed)



Linear Systems



- Input/output linearity at $x(0) = 0$
 - Linear systems are linear in initial condition and input \Rightarrow need to use $x(0) = 0$ to add outputs together
 - For different initial conditions, you need to be more careful
- Linear system \Rightarrow step response and frequency response scale with input amplitude
 - 2X input \Rightarrow 2X output
 - Allows us to use ratios and percentages in step or frequency response. *These are independent of input amplitude*
 - Limitation: input saturation \Rightarrow only holds up to certain input amplitude

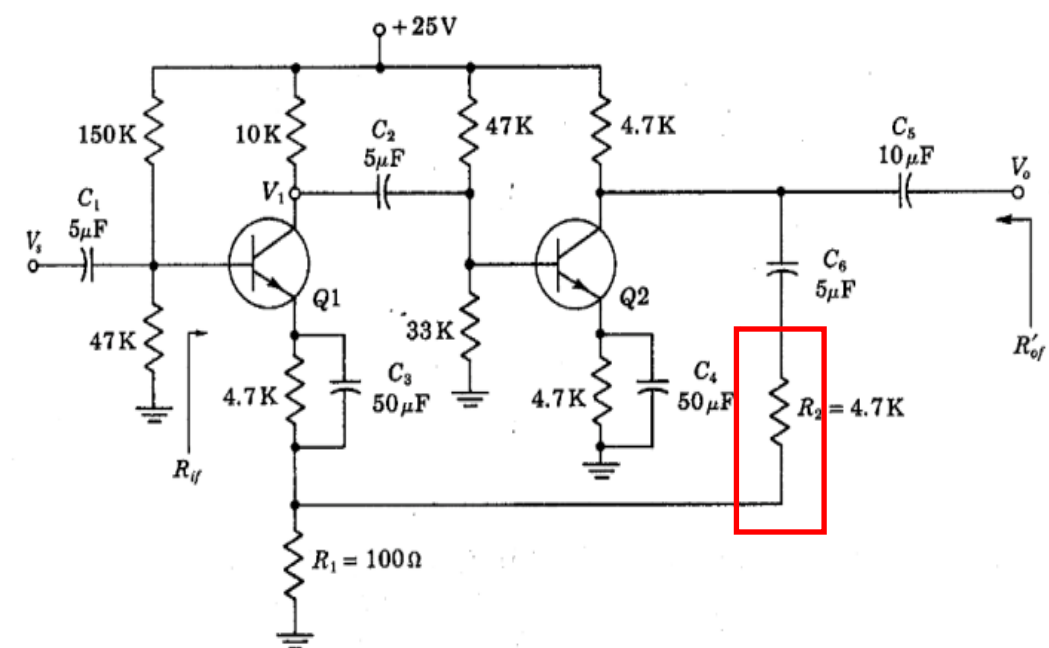
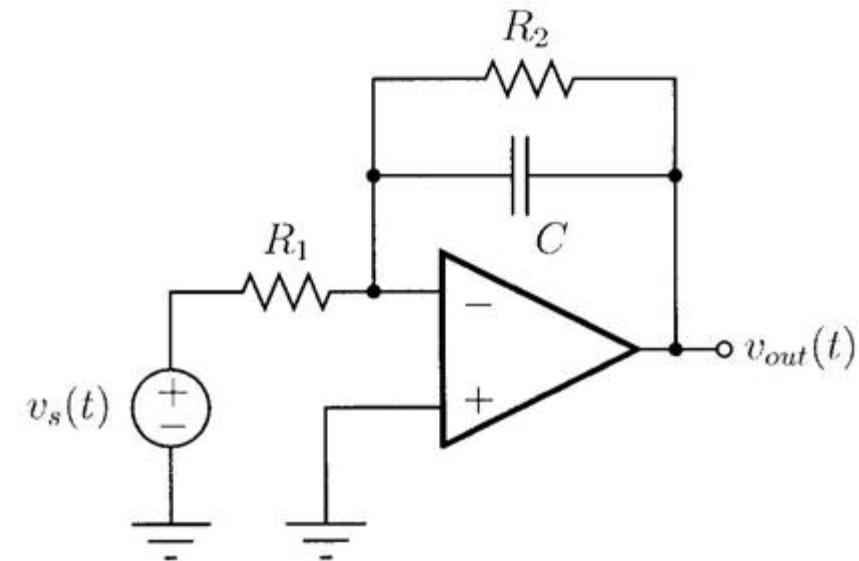
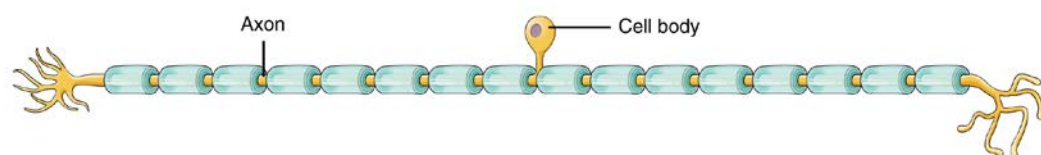
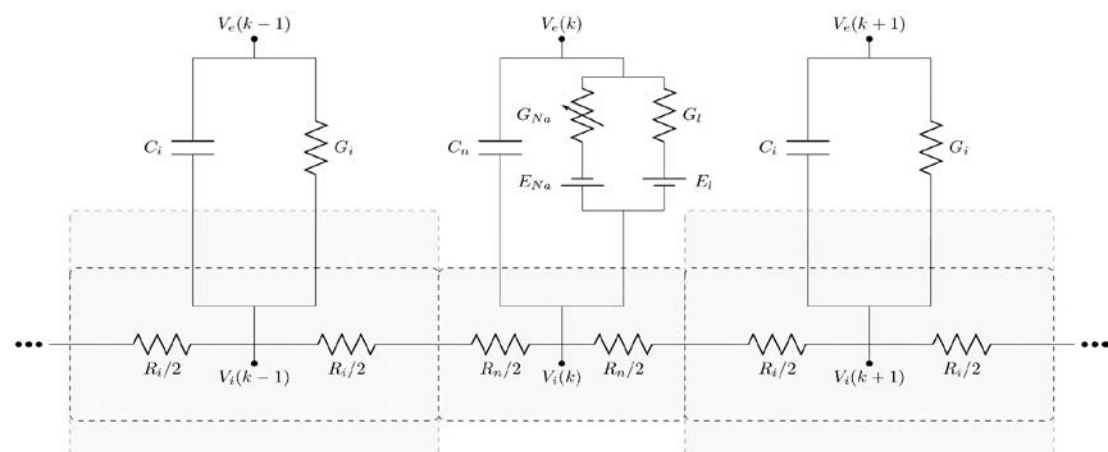
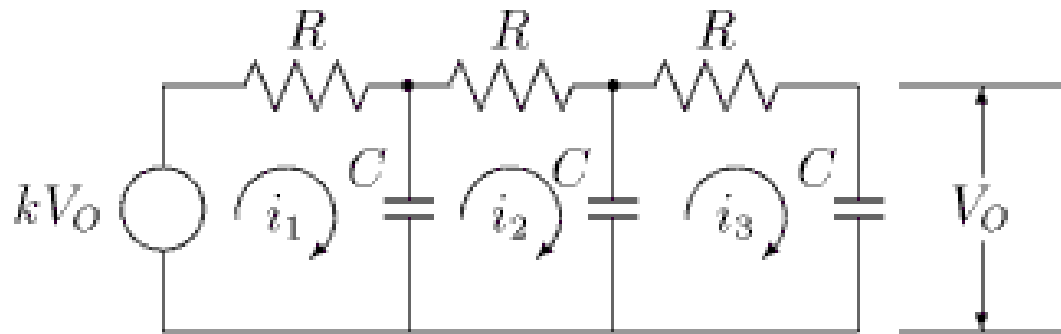




Why are Linear Systems Important?

Many important *examples*

- Electronic circuits



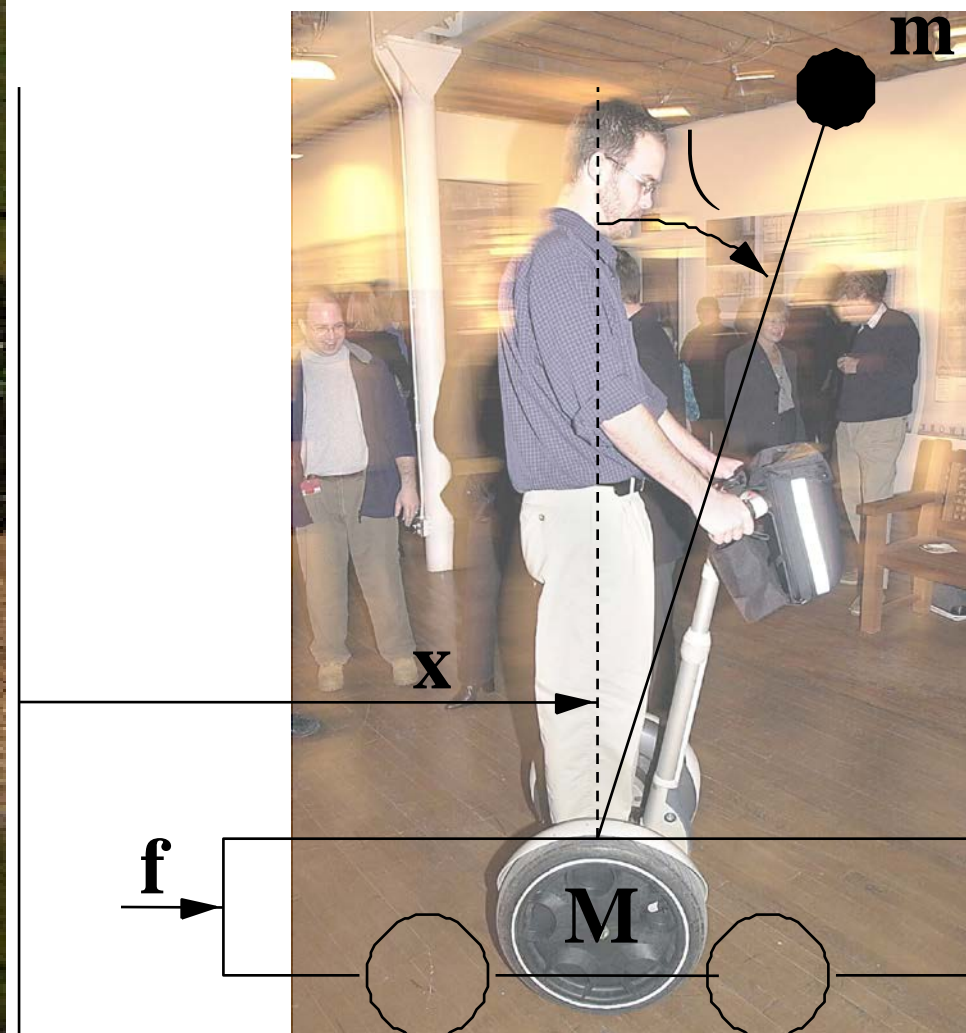
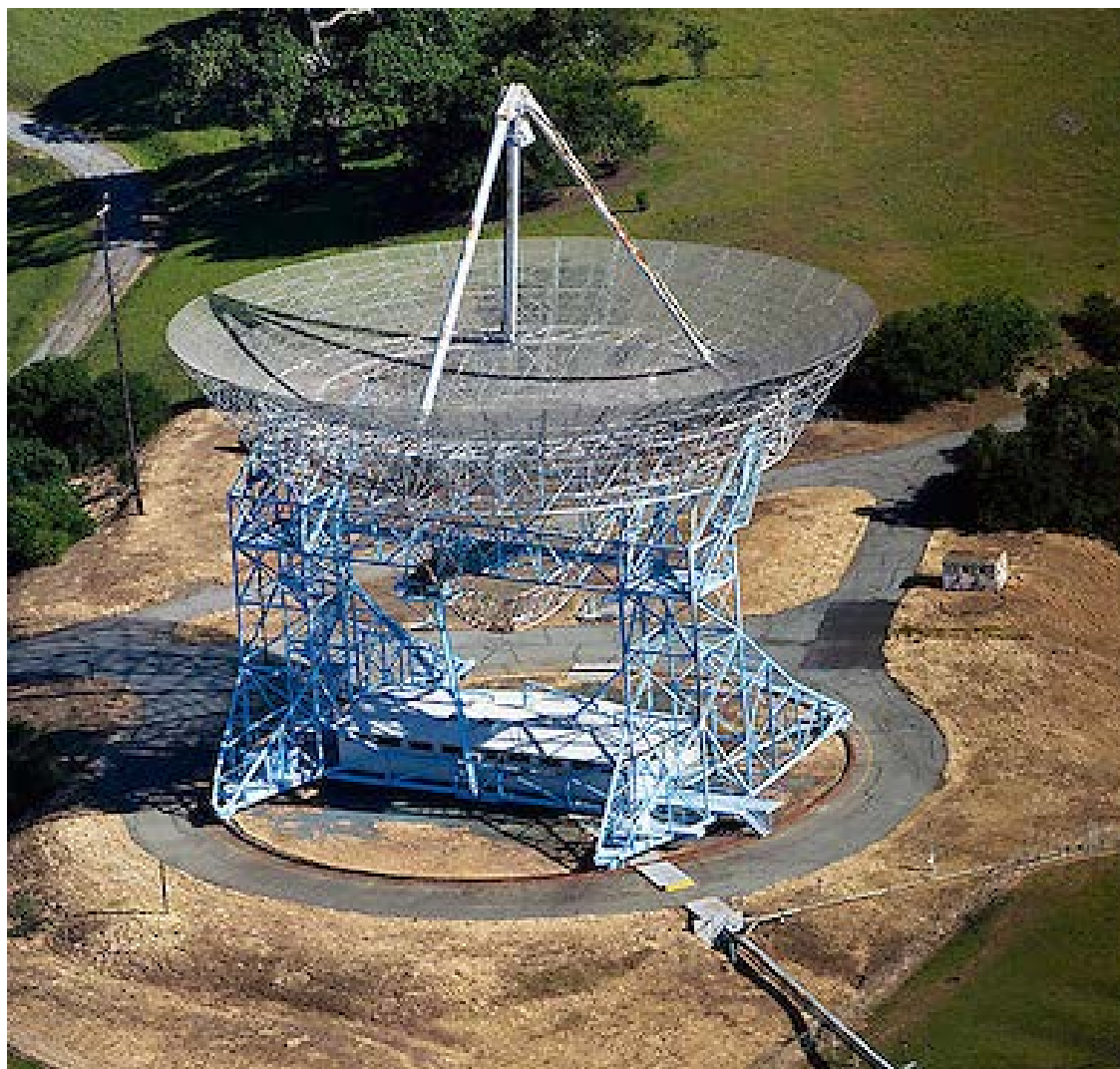
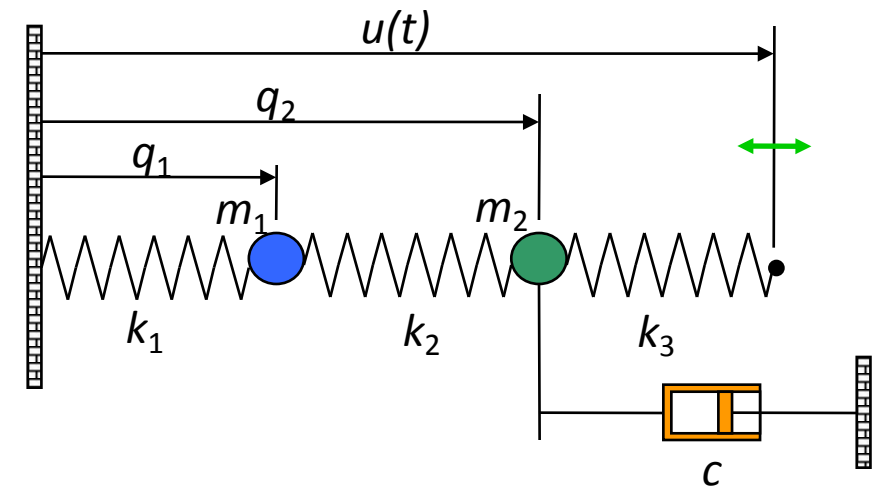
- Especially true after **feedback**
- Frequency response is key performance specification



Why are Linear Systems Important?

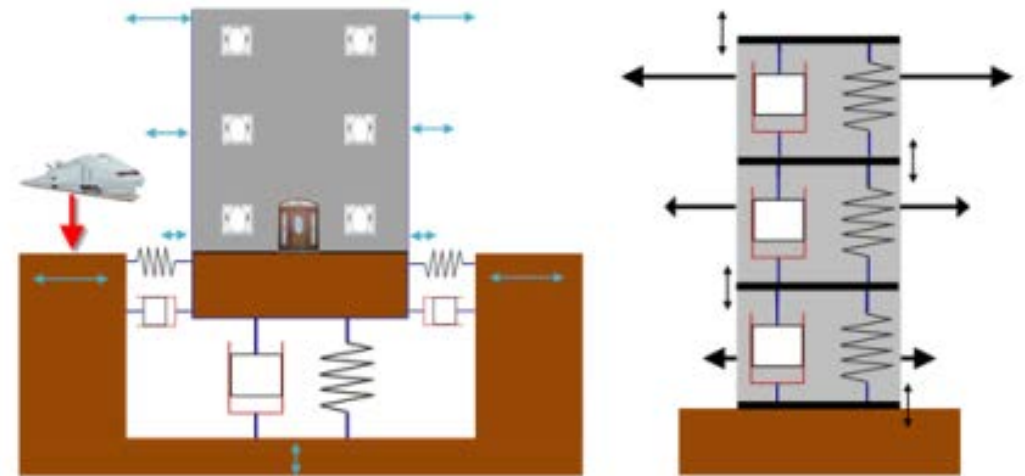
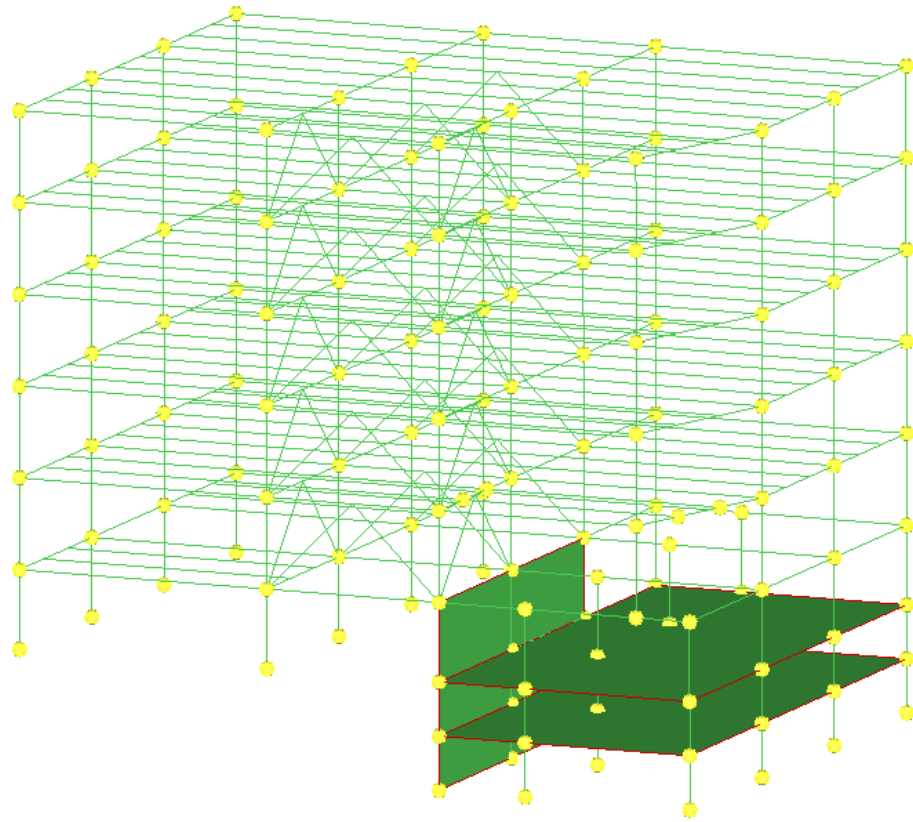
Many important *examples*

- Mechanical Systems





Why are Linear Systems Important?

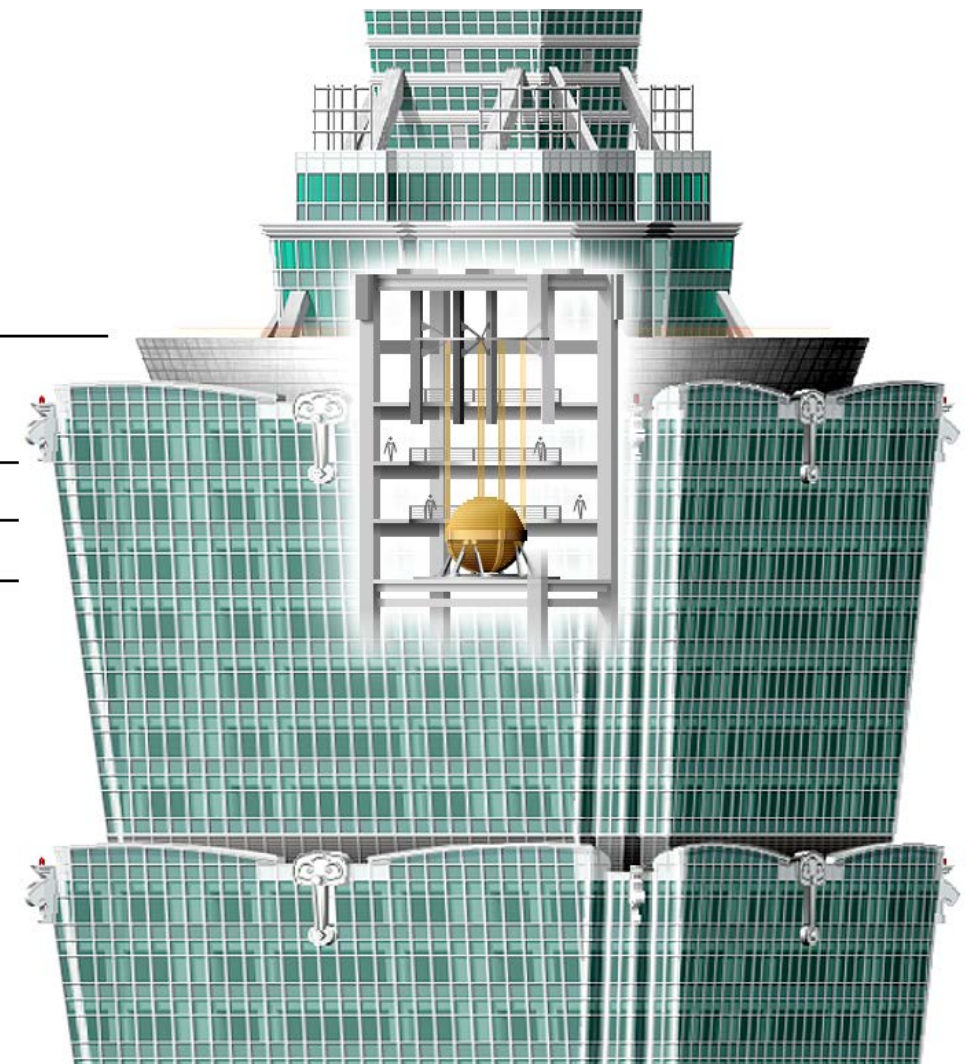


91st Floor [390.60 m]
(Outdoor Observation Deck)

89th Floor [382.20 m]
(Indoor Observation Deck)

88th Floor

87th Floor

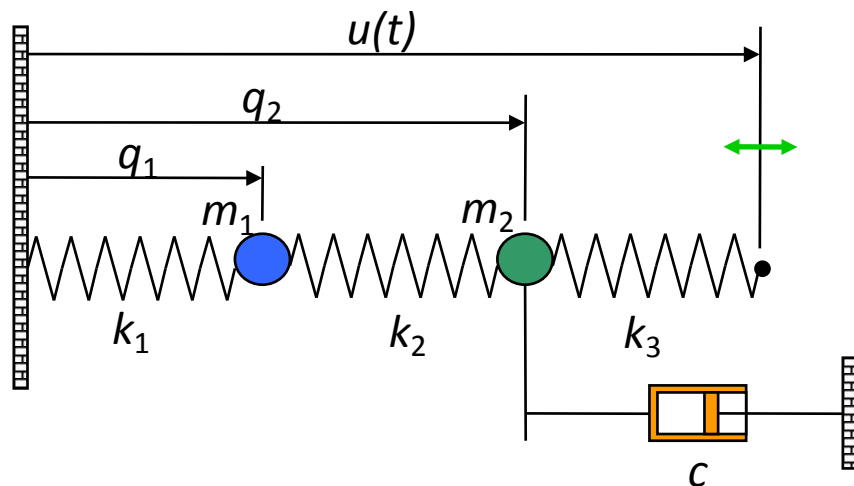
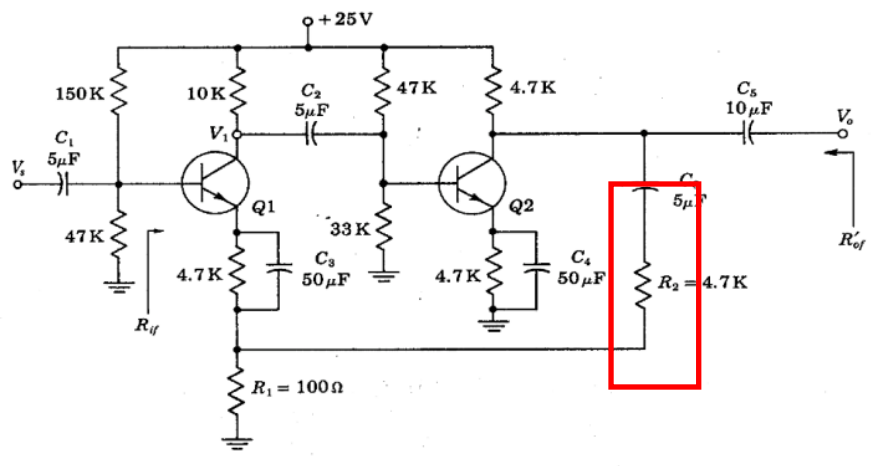




Why are Linear Systems Important?

Many important *examples*

- Electronic circuits



Many important *tools*

- Frequency and step response,
 - Traditional tools of control theory
 - Developed in 1930's at Bell Labs

- Classical control design toolbox
 - Nyquist plots, gain/phase margin
 - Loop shaping

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110

- Optimal control and estimators
 - Linear quadratic regulators
 - Kalman estimators

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- Robust control design
 - H_1 control design
 - μ analysis for structured uncertainty

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213



Solutions of Linear Time Invariant Systems: The Matrix Exponential

Linear Time Invariant (LTI) System:

- If *Linear System* input $u(t)$ leads to output $y(t)$
- If $u(t+T)$ leads to output $y(t+T)$, the system is *time invariant*

Scalar LTI system, with no input

$$\begin{array}{l} \dot{x} = ax \\ y = cx \end{array} \quad x(0) = x_0 \quad \longrightarrow \quad x(t) = e^{at} x_0 \quad \longrightarrow \quad y(t) = ce^{at} x_0$$

- Matrix LTI system, with no input

$$\begin{array}{l} \dot{x} = Ax \\ y = Cx \end{array} \quad x(0) = x_0 \quad \longrightarrow \quad x(t) = e^{At} x_0 \quad \longrightarrow \quad y(t) = Ce^{At} x_0$$

Matrix Exponential



The Matrix Exponential

Recall scalar exponential formula:

$$- e^x = 1 + \frac{x}{1!} + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots, \quad -\infty < x < \infty$$

Matrix exponential defined analogously:

$$- e^M = I + \frac{1}{1!}M + \frac{1}{2!}M^2 + \frac{1}{3!}M^3 + \dots = \sum_{k=0}^{\infty} \frac{1}{k!}M^k$$

Some useful properties of the Matrix Exponential

- If $M = \begin{bmatrix} m_{11} & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & m_{nn} \end{bmatrix}$, then $e^M = \begin{bmatrix} e^{m_{11}} & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & e^{m_{nn}} \end{bmatrix}$
- If matrix Y is invertible, then $e^{YMY^{-1}} = Ye^MY^{-1}$
- If M is diagonalizable ($M = TDT^{-1}$), then $e^M = Te^DT^{-1}$



The Convolution Integral: Step 1

Let $H(t)$ denote the response of a LTI system to a **unit step** input at $t=0$.

- Assuming the system starts at Equilibrium

The response to the steps are:

- First step input at time $t=0$: $H(t - t_0)u(t_0)$
- Second step input at time t_1 : $H(t - t_1)(u(t_1) - u(t_0))$
- Third step input at time t_2 : $H(t - t_2)(u(t_2) - u(t_1))$

By linearity, we can add the response

$$\begin{aligned} y(t) &= H(t - t_0)u(t_0) + H(t - t_1)(u(t_1) - u(t_0)) + \dots \\ &= (H(t - t_0) - H(t - t_1))u(t_0) + (H(t - t_1) - H(t - t_2))u(t_1) + \dots \\ &= \sum_{n=0}^{t_0 < t} \frac{H(t - t_n) - H(t - t_{n+1})}{t_{n+1} - t_n} u(t_n)(t_{n+1} - t_n) \end{aligned}$$

Taking the limit as $(t_{n+1} - t_n) \rightarrow 0$

$$y(t) = \int_0^t H'(t - \tau)u(\tau)d\tau$$

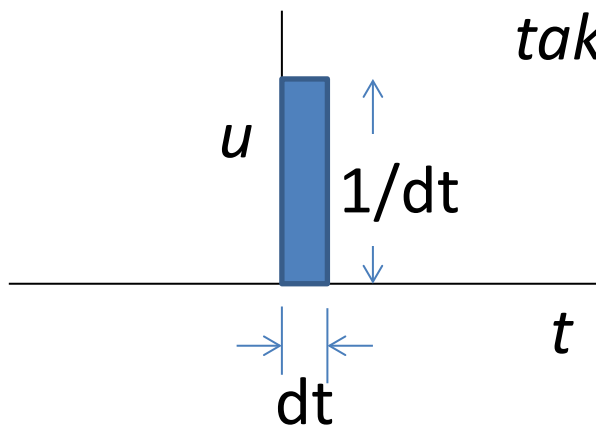


Impulse Response

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned} \longrightarrow y(t) = \underbrace{Ce^{At}x(0)}_{\text{homogeneous}} + ???$$

- What is the “impulse response” due to $u(t)=\delta(t)$?

take limit as $dt \rightarrow 0$ but keep unit area



- Apply this unit impulse to the system (with $x(0)=0$):

$$x(0^+) = \int_{0^-}^{0^+} (Ax + Bu) dt = B$$

$$\Rightarrow x(t) = e^{At}B$$

- Analogous to discrete-time response to input at time zero



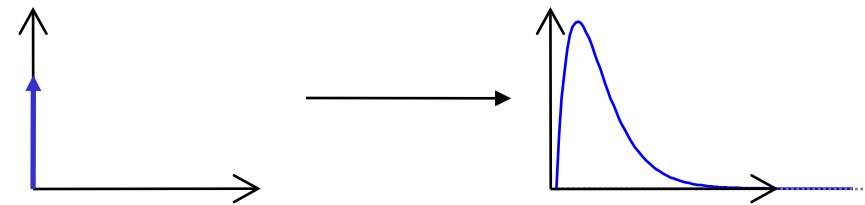
Response to inputs: Convolution

$$\dot{x} = Ax + Bu$$

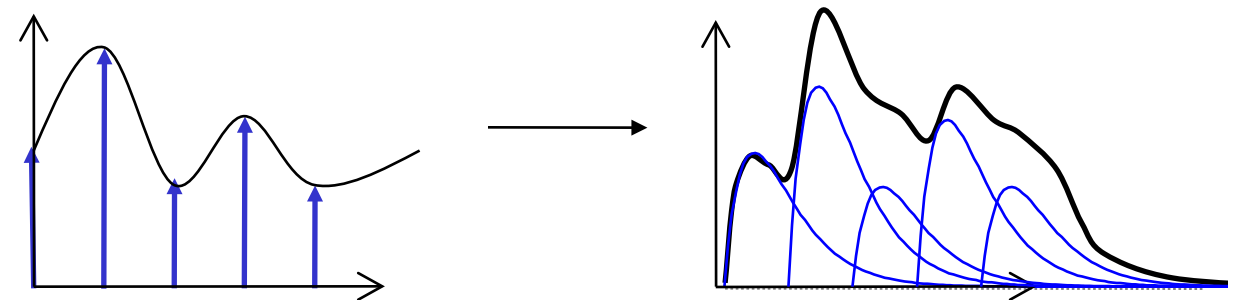
$$y = Cx + Du$$

$$\longrightarrow y(t) = \underbrace{Ce^{At}x(0)}_{\text{homogeneous}} + ???$$

- Impulse response, $h(t) = Ce^{At}B$
 - Response to input “impulse”
 - Equivalent to “Green’s function”



- Linearity \Rightarrow compose response to arbitrary $u(t)$ using *convolution*
 - Decompose input into “sum” of shifted impulse functions
 - Compute impulse response for each
 - “Sum” impulse response to find $y(t)$
 - Take limit as $dt \rightarrow 0$
- Complete solution: use integral instead of “sum”



$$y(t) = Ce^{At}x(0) + \int_{\tau=0}^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

- linear with respect to initial condition *and* input
- 2X input \Rightarrow 2X output when $x(0) = 0$

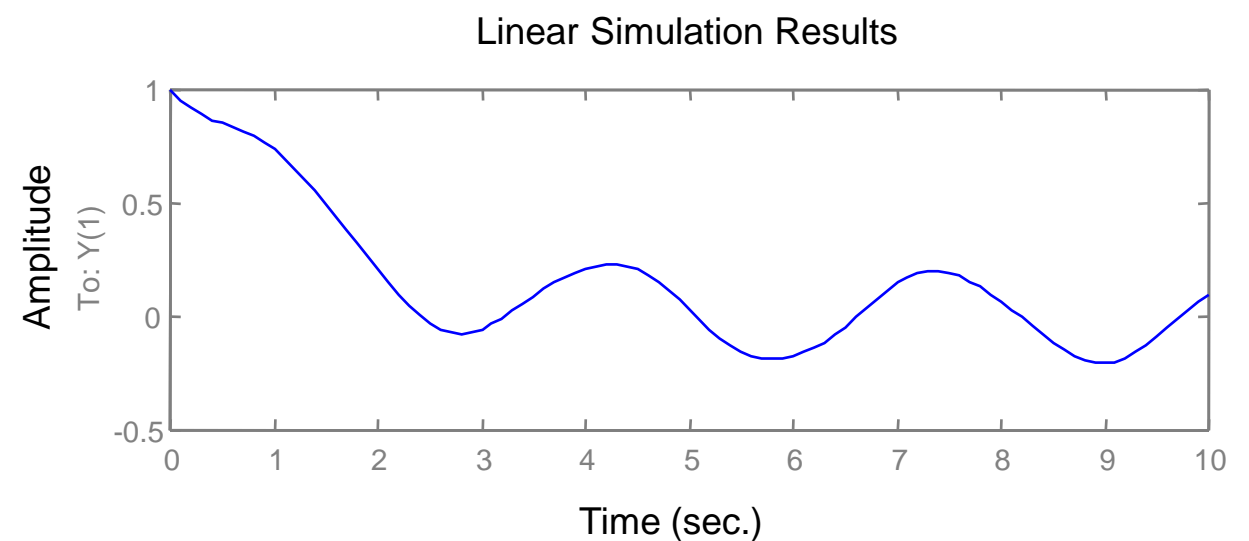
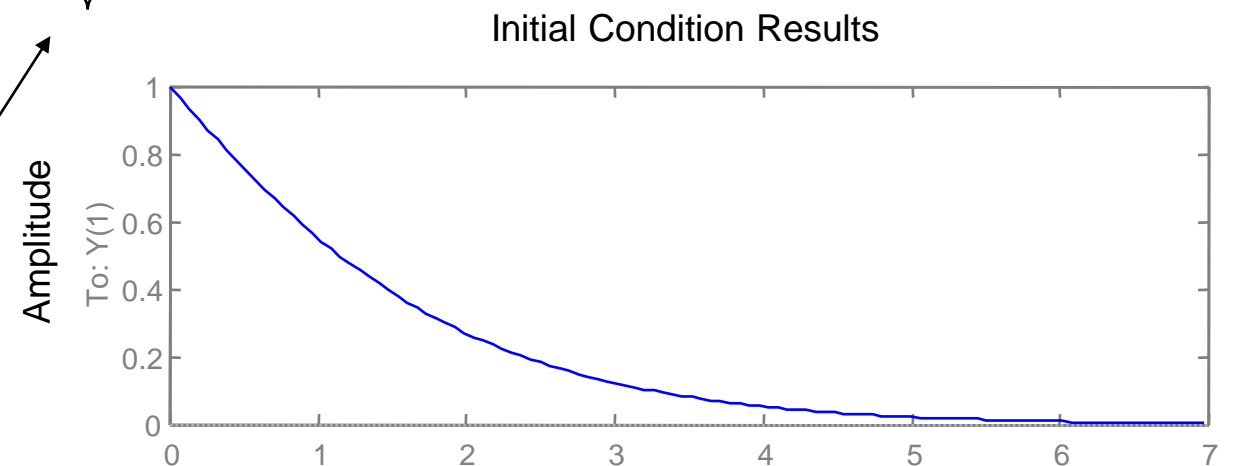
Matlab/Python Tools for Linear Systems

$$y(t) = \underbrace{C e^{At} x(0)}_{\text{Initial Condition Results}} + \underbrace{\int_{\tau=0}^t C e^{A(t-\tau)} B u(\tau) d\tau + D u(t)}_{\text{Linear Simulation Results}}$$

```
A = [-1 1; 0 -1]; B = [0; 1];  
C = [1 0]; D = [0];  
x0 = [1; 0.5];
```

```
sys = ss(A,B,C,D);  
initial(sys, x0);  
impulse(sys);
```

```
t = 0:0.1:10;  
u = 0.2*sin(5*t) + cos(2*t);  
lsim(sys, u, t, x0);
```



- Other MATLAB commands

- gensig, square, sawtooth – produce signals of diff. types
- step, impulse, initial, lsim – time domain analysis
- bode, freqresp, evalfr – frequency domain analysis

ltiview – linear
time invariant
system plots

Input/Output Performance

Return to system with inputs

- How does system response to changes in input values?



Transient response:

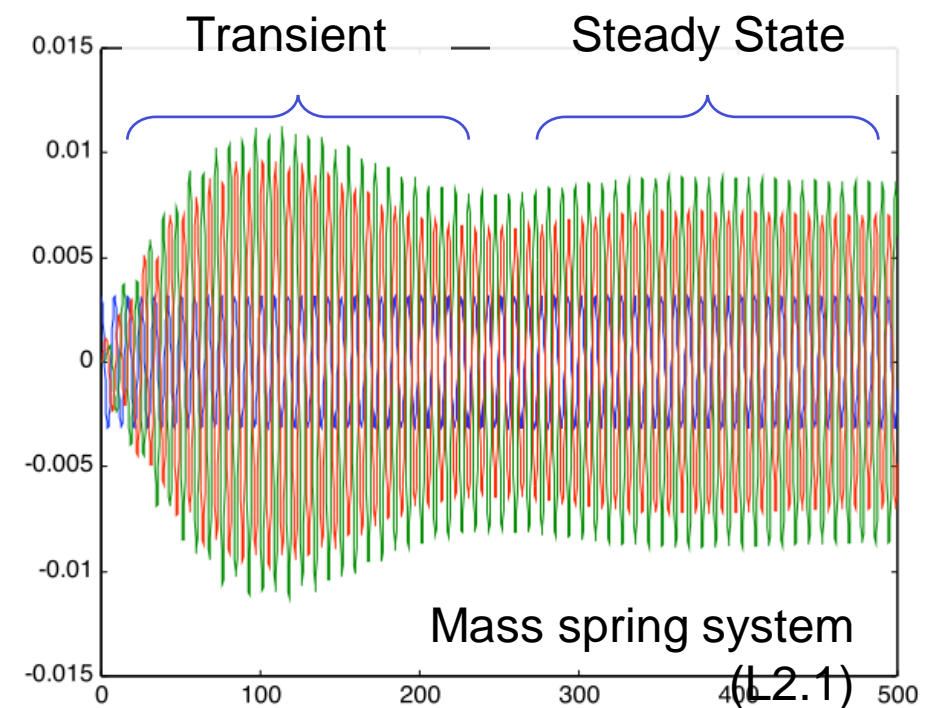
- What happens right after a new input is applied

Steady state response:

- What happens a long time after the input is applied

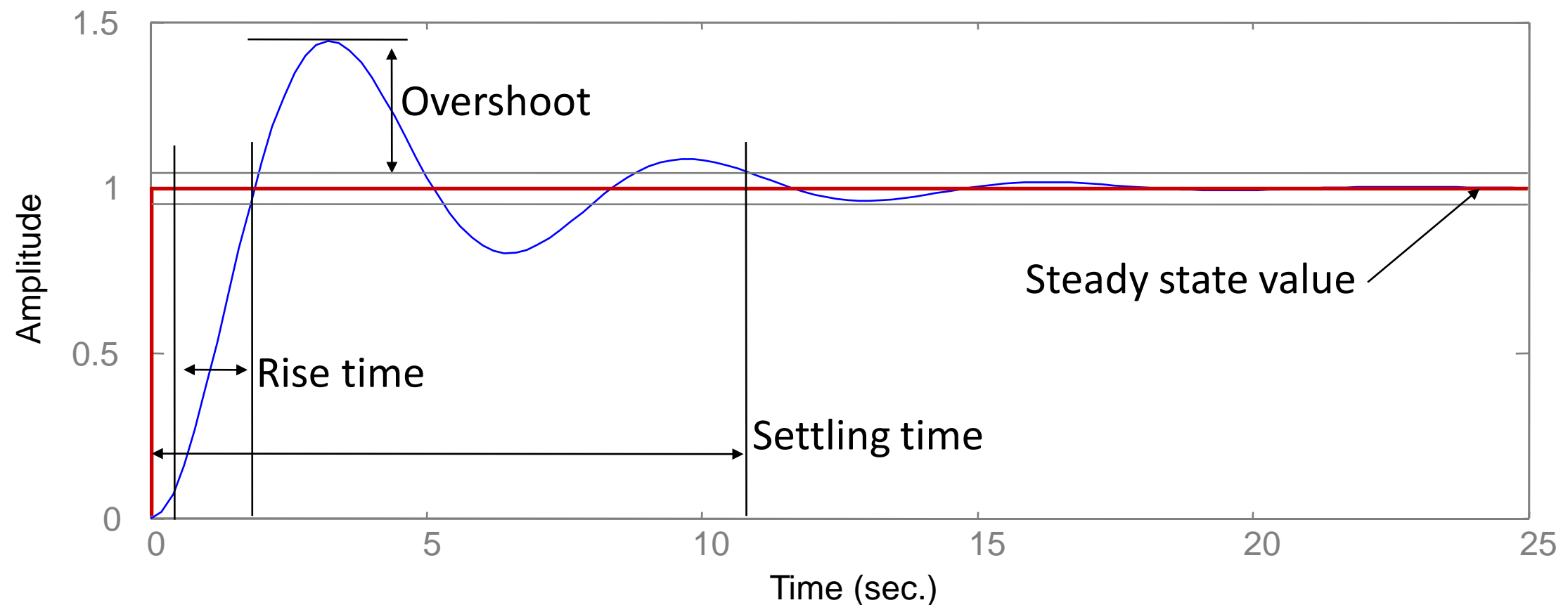
Stability vs input/output performance

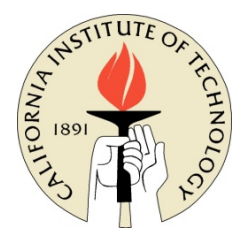
- Systems that are close to instability typically exhibit poor input/output performance
- Nearly unstable systems (slow convergence) often exhibit “ringing” (highly oscillatory response to [non-periodic] inputs)



Step Response

- Output characteristics in response to a “step” input
 - Rise time: time required to move from 5% to 95% of final value
 - Overshoot: ratio between amplitude of first peak and steady state value
 - Settling time: time required to remain w/in $p\%$ (usually 2%) of final value
 - Steady state value: final value at $t = \infty$





Second Order Systems

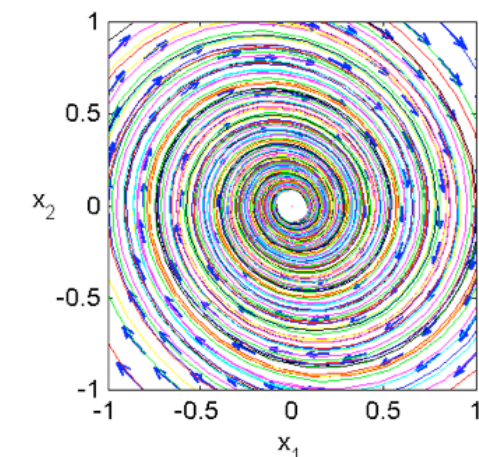
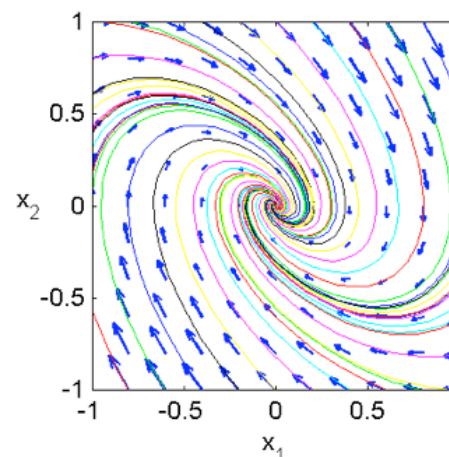
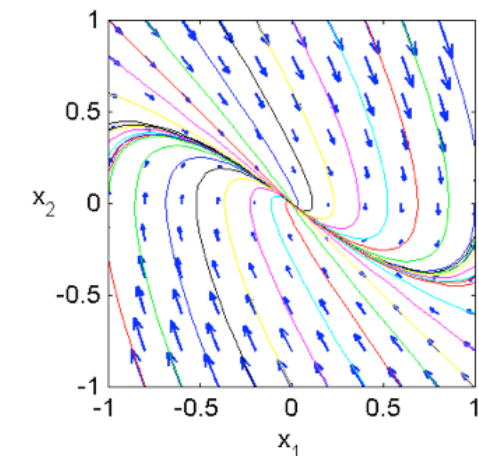
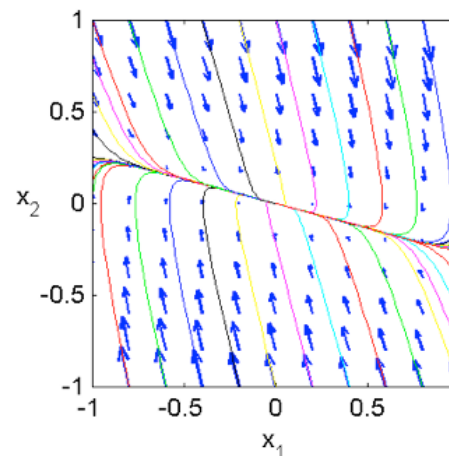
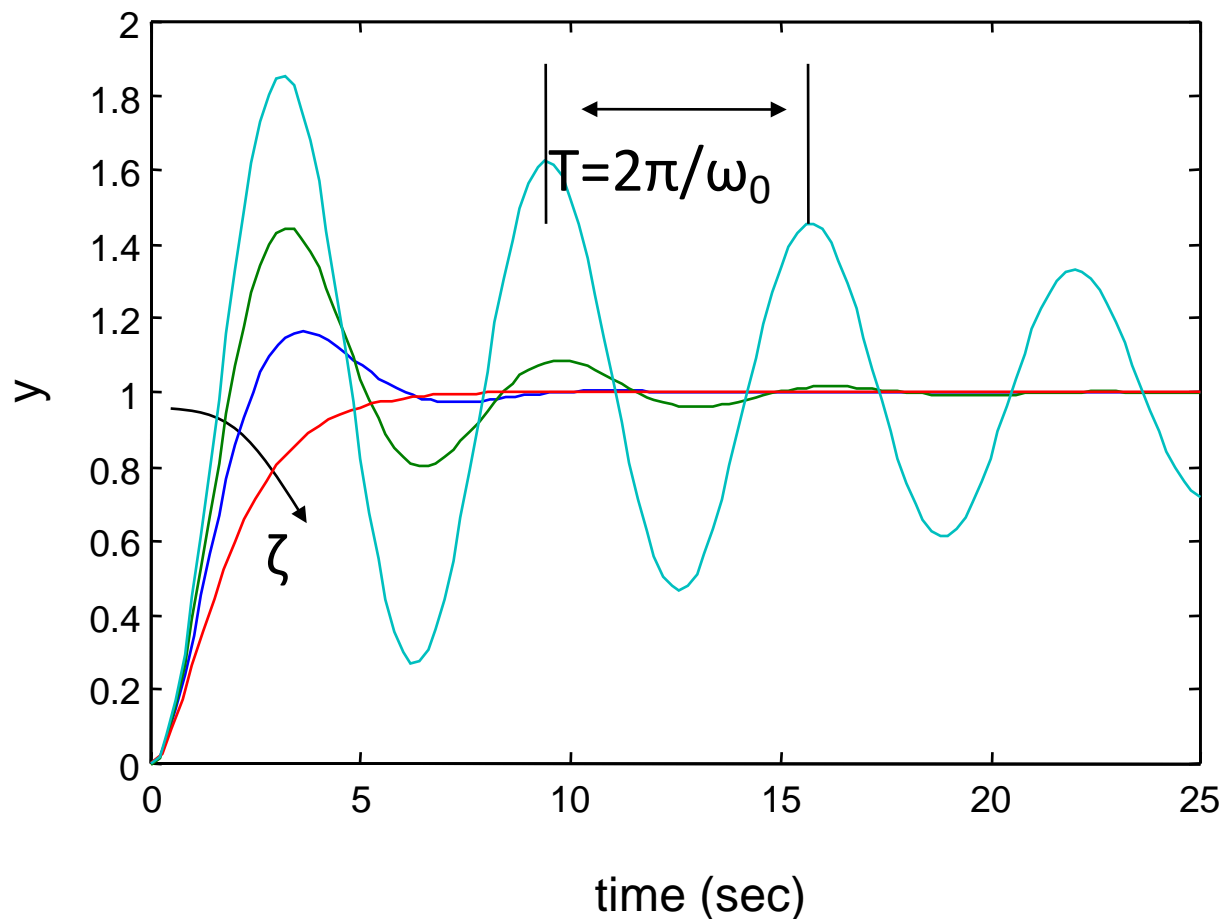
- Many important examples:
- Insight to response for higher orders (eigenvalues of A are either real or complex)
 - Exception is non-diagonalizable A (non-trivial Jordan form)

$$\ddot{q} + 2\zeta\omega_0\dot{q} + \omega_0^2 q = u \quad \leftrightarrow$$

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\omega_0^2 & -2\zeta\omega_0 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

For $\zeta < 1$, eigenvalues at

$$\left(-\zeta \pm j\sqrt{1 - \zeta^2} \right) \omega_0$$



- Analytical formulas exist for overshoot, rise time, settling time, etc
- Will study more next week

Stability of Linear Systems

$$\begin{aligned} \dot{x} &= Ax + Bu \\ \cancel{y} &= \cancel{Cx + Du} \end{aligned}$$

$$x(t) = e^{At} x_0$$

Q: when is the system asymptotically stable?

$$\lim_{t \rightarrow \infty} x(t) = 0$$

Stability is determined by the *eigenvalues* of the matrix A

- Simple case: diagonal system

$$\dot{x} = \begin{bmatrix} \lambda_1 & & 0 \\ & \ddots & \\ 0 & & \lambda_n \end{bmatrix} x \quad \textcircled{R} \quad x(t) = \begin{bmatrix} e^{\lambda_1 t} & & 0 \\ & \ddots & \\ 0 & & e^{\lambda_n t} \end{bmatrix} x_0$$

Stable if $\lambda_i \leq 0$
 Asy stable if $\lambda_i < 0$
 Unstable if $\lambda_i > 0$

- More generally: transform to “Jordan” form

$$\dot{x} = T^{-1} J T x \quad J = \begin{bmatrix} J_1 & & 0 \\ & \ddots & \\ 0 & & J_k \end{bmatrix} \quad J_i = \begin{bmatrix} \lambda_i & 1 & 0 \\ & \ddots & 1 \\ 0 & & \lambda_i \end{bmatrix}$$

Asy stable if $\text{Re}(\lambda_i) < 0$
 Unstable if $\text{Re}(\lambda_i) > 0$
Indeterminate if $\text{Re}(\lambda_i) = 0$

Form of eigenvalues determines system behavior

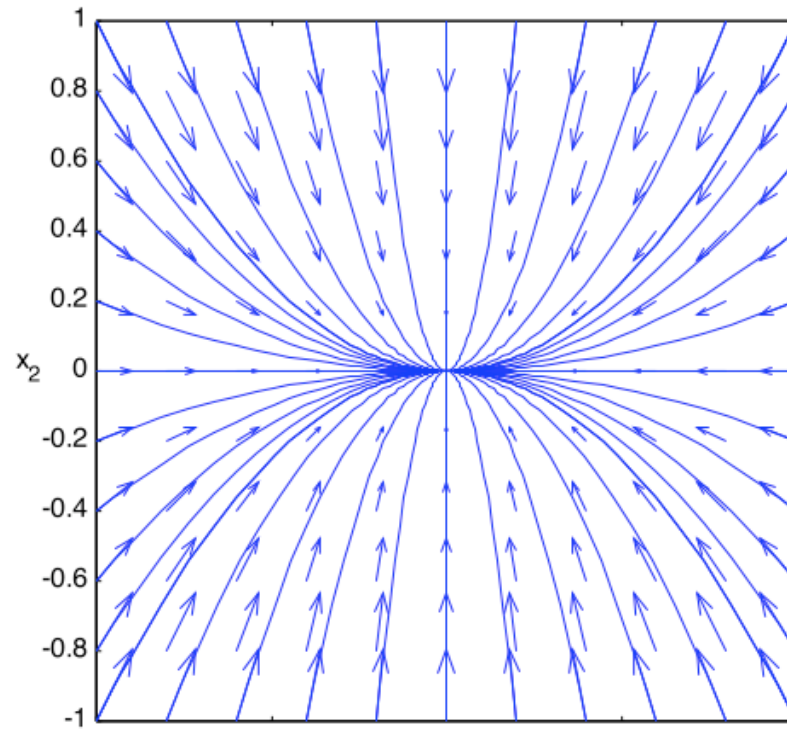
Linear systems are automatically *globally* stable or unstable



Eigenstructure of Linear Systems

Real e-values

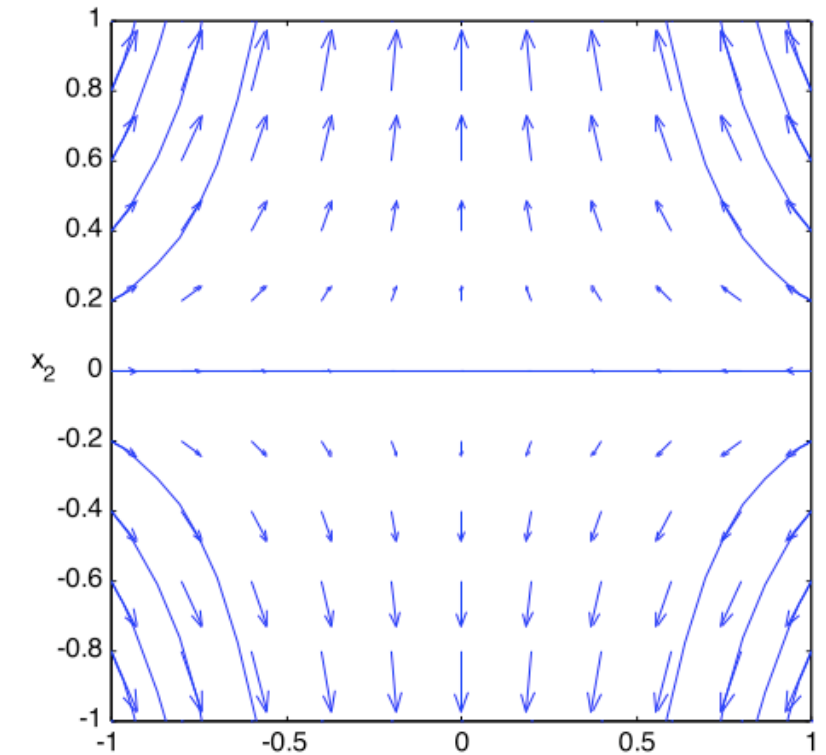
$$\operatorname{Re}(\lambda_i) < 0$$



Real e-values

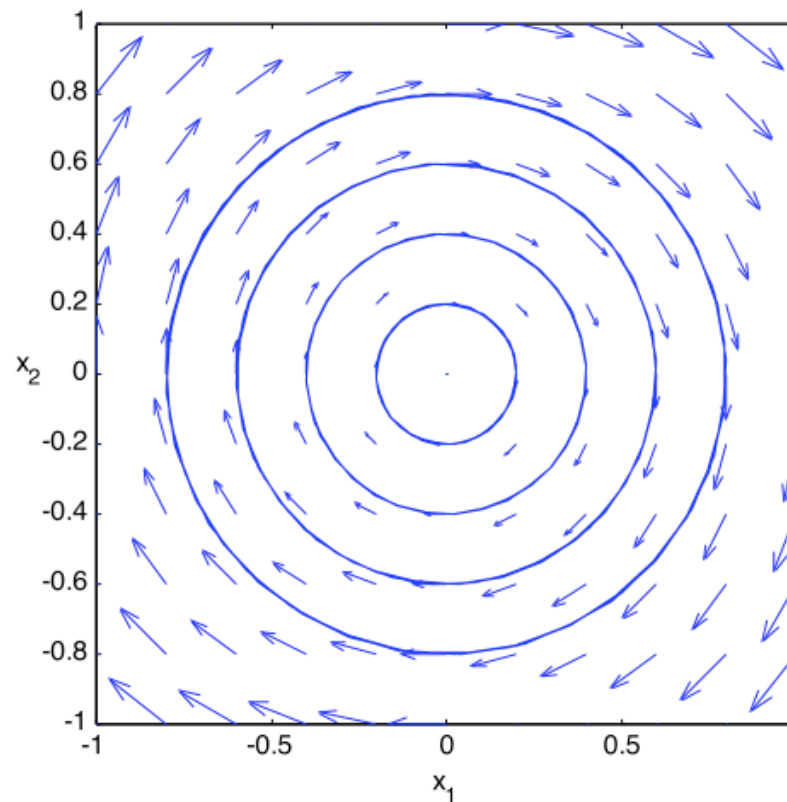
$$\operatorname{Re}(\lambda_i) < 0$$

$$\operatorname{Re}(\lambda_i) > 0$$



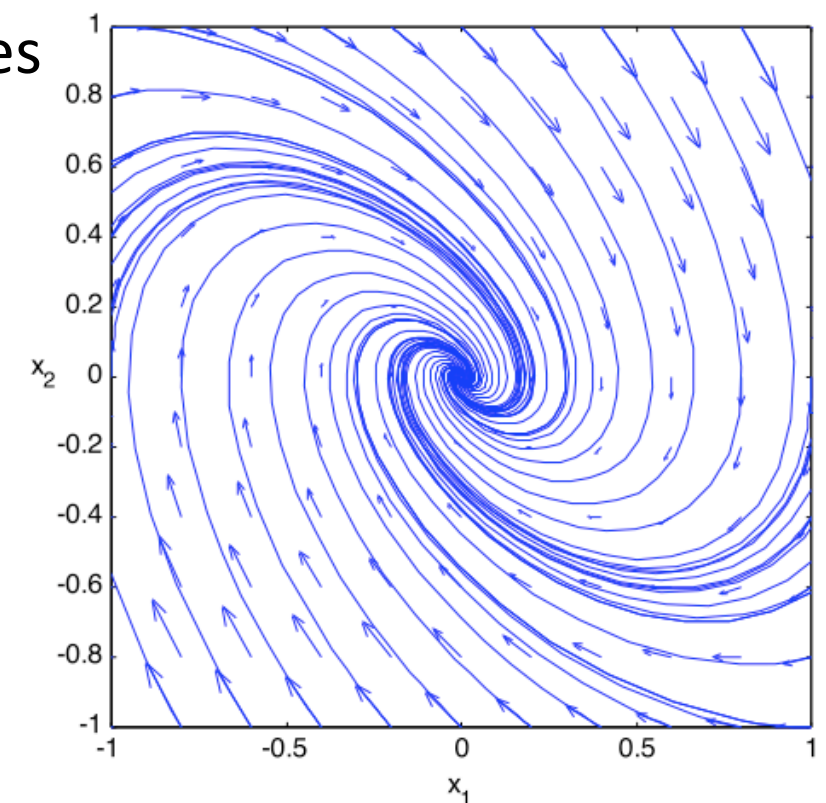
Complex e-values

$$\operatorname{Re}(\lambda_i) = 0$$



Complex e-values

$$\operatorname{Re}(\lambda_i) < 0$$

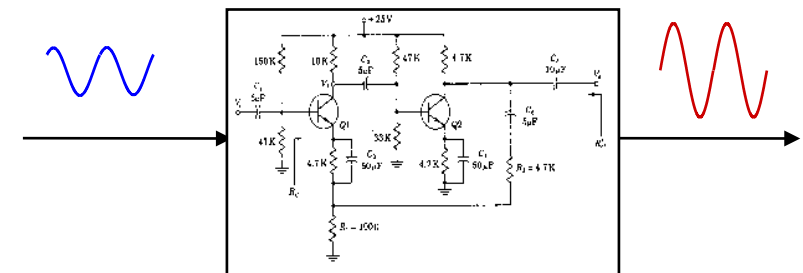




Frequency Response

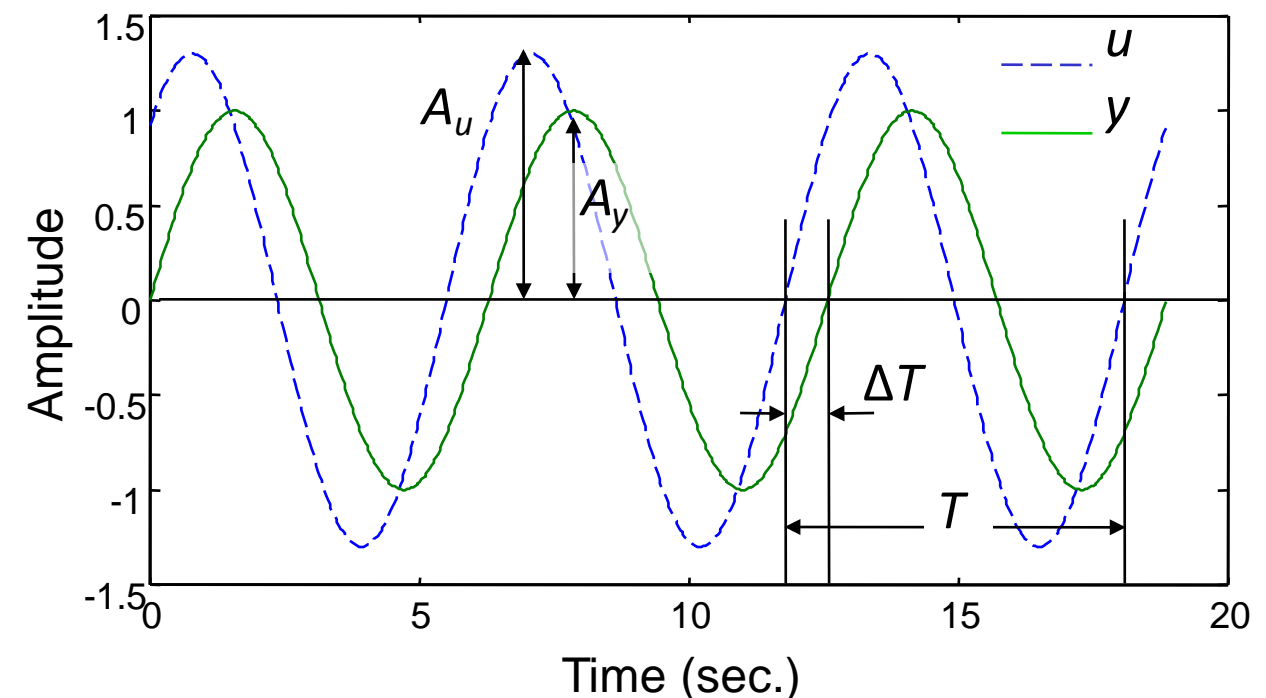
- Measure *steady state* response of system to sinusoidal input

- Example: audio amplifier – would like consistent (“flat”) amplification between 20 Hz & 20,000 Hz
- Individual sinusoids are good *test signals* for measuring performance in many systems



- Approach: plot input and output, measure *relative* amplitude and phase

- Use MATLAB or SIMULINK to generate response of system to sinusoidal output
- Gain = A_y/A_u
- Phase = $2\pi \cdot \Delta T/T$



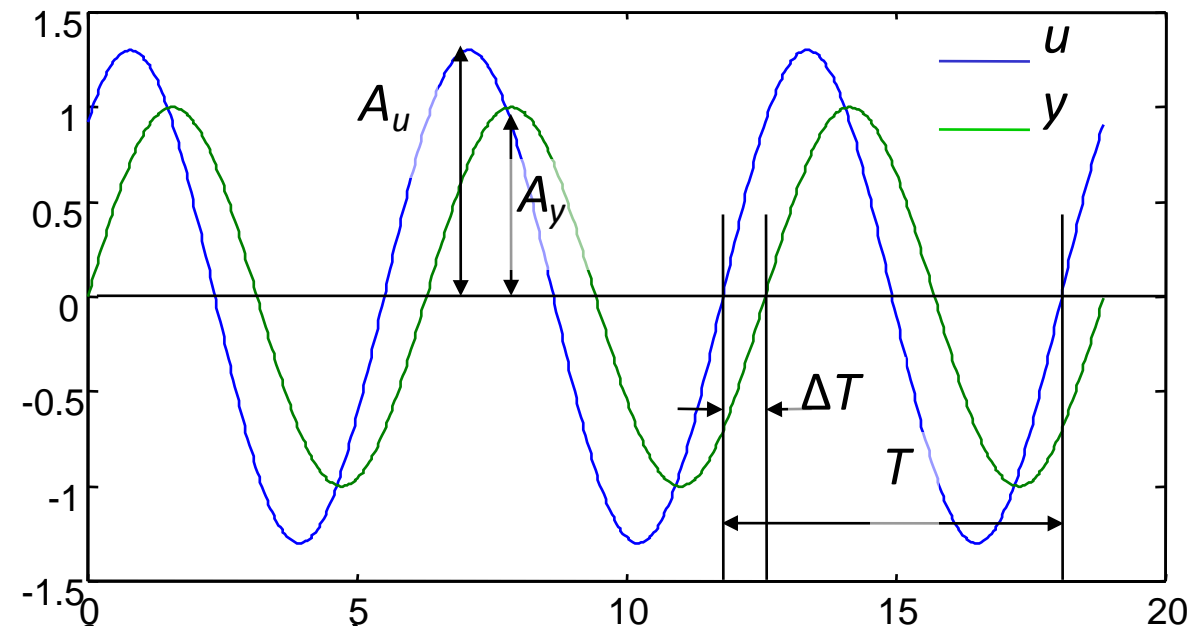
- May not work for *nonlinear* systems

- System nonlinearities can cause *harmonics* to appear in the output
- Amplitude and phase may not be well-defined
- For *linear* systems, frequency response is always well defined



Computing Frequency Responses

- Technique #1: plot input and output, measure relative amplitude and phase
 - Generate response of system to sinusoidal output
 - Gain = A_y/A_u
 - Phase = $2\pi \cdot \Delta T/T$
 - For *linear* system, gain and phase don't depend on the input amplitude



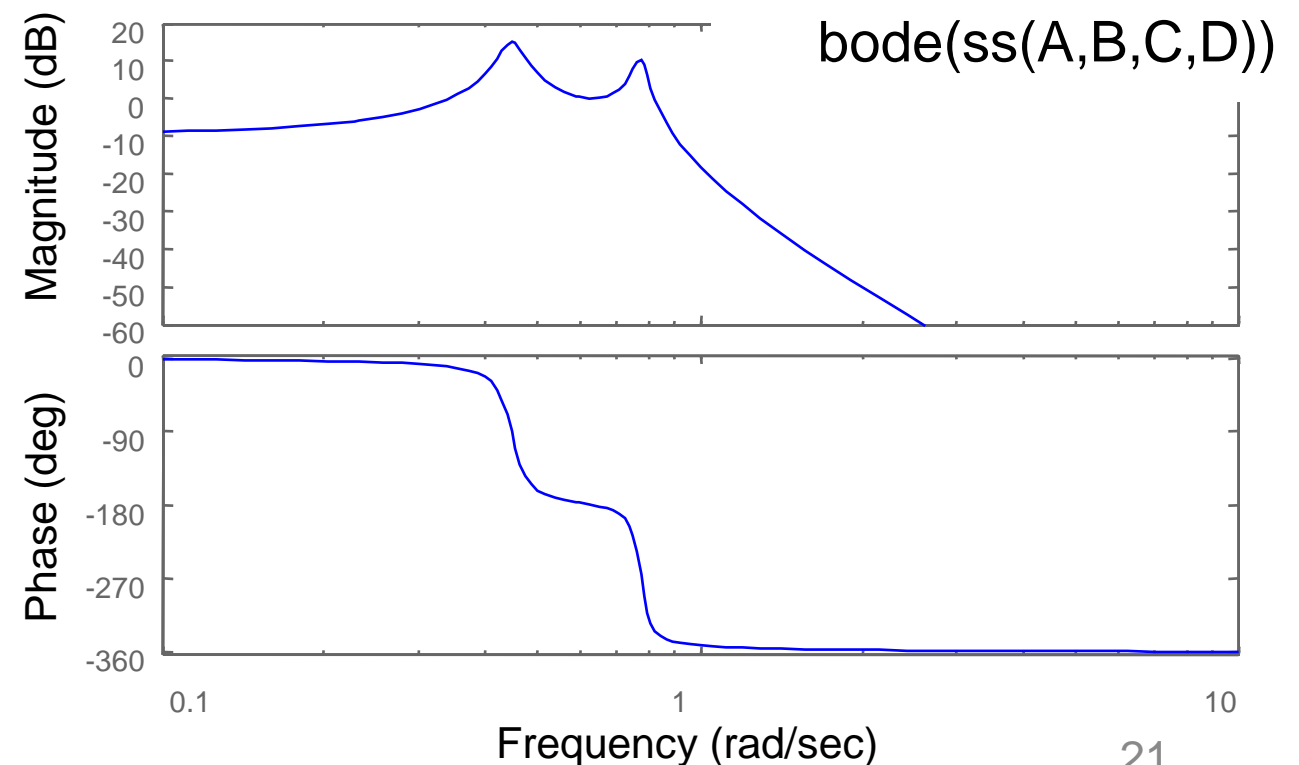
- Technique #2 (linear systems): use bode (or freqresp) command

- Assumes linear dynamics in state space form:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

- Gain plotted on log-log scale
 - $\text{dB} = 20 \log_{10}(\text{gain})$
- Phase plotted on linear-log scale





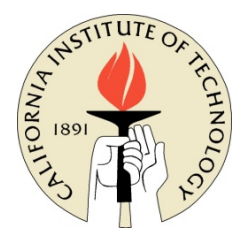
Calculating Frequency Response from convolution equation... (more later)

- Convolution equation describes response to any input; use this to look at response to sinusoidal input:

$$u(t) = A \sin(\omega t) = \frac{A}{2i} (e^{i\omega t} - e^{-i\omega t})$$

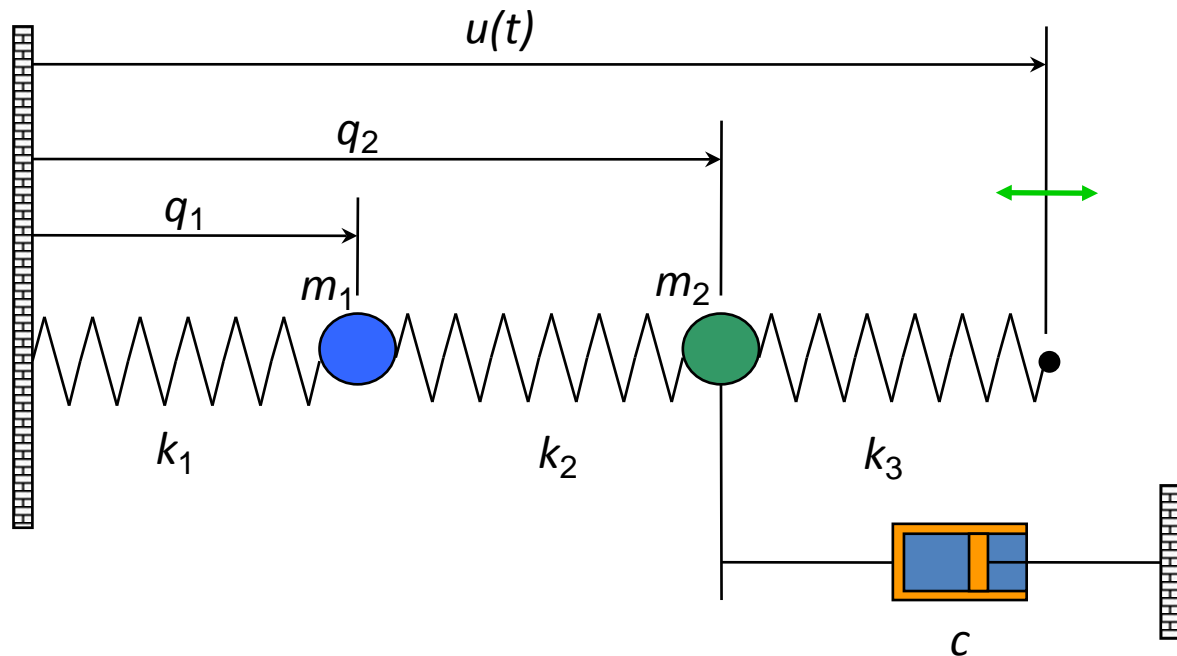
$$\begin{aligned} x(t) &= e^{At} x(0) + \int_0^t e^{A(t-\tau)} B e^{i\omega\tau} d\tau \\ &= e^{At} x(0) + e^{At} \int_0^t e^{(i\omega I - A)\tau} B d\tau \\ &= e^{At} x(0) + e^{At} (i\omega I - A)^{-1} e^{(i\omega I - A)\tau} \Big|_{\tau=0}^t B \\ &= e^{At} x(0) + e^{At} (i\omega I - A)^{-1} (e^{(i\omega I - A)t} - I) B \\ &= \underbrace{e^{At} (x(0) - (i\omega I - A)^{-1} B)}_{\text{Transient (decays if stable)}} + \underbrace{(i\omega I - A)^{-1} B e^{i\omega t}}_{\text{Ratio of response/input}} \end{aligned}$$

$$\begin{aligned} y(t) &= Cx(t) + Du(t) \\ &= C e^{At} (x(0) - (i\omega I - A)^{-1} B) + \boxed{(C(i\omega I - A)^{-1} B + D)} e^{i\omega t} \\ &\quad \text{"Frequency response"} \end{aligned}$$



Spring Mass System

Frequency response:
 $C(j\omega I - A)^{-1}B + D$



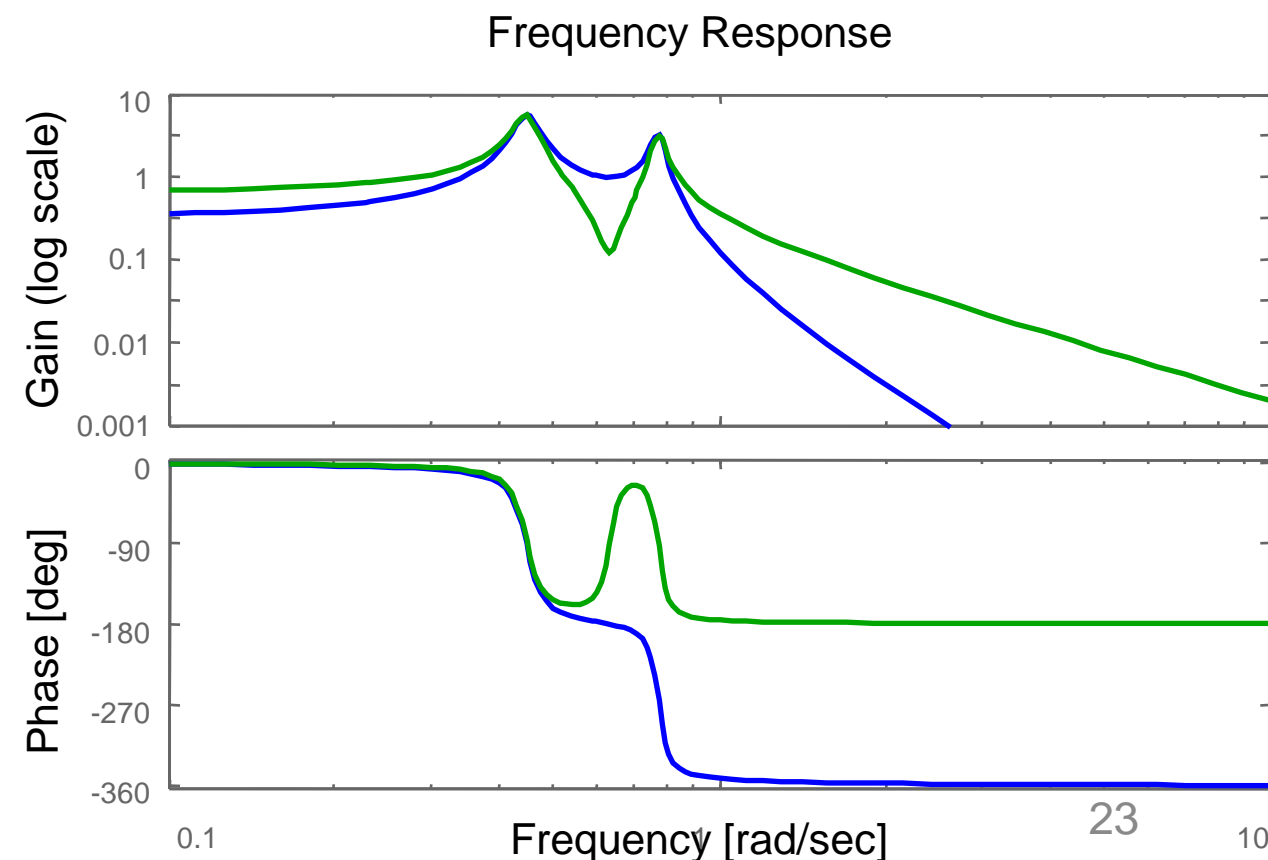
$$\frac{d}{dt} \begin{bmatrix} q_1 \\ q_2 \\ \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\frac{k_1+k_2}{m} & \frac{k_2}{m} & 0 & 0 \\ \frac{k_2}{m} & -\frac{k_2+k_3}{m} & 0 & -\frac{c}{m} \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

With $k_1 = k_2 = 1$, $m = 1$, $c = 0$

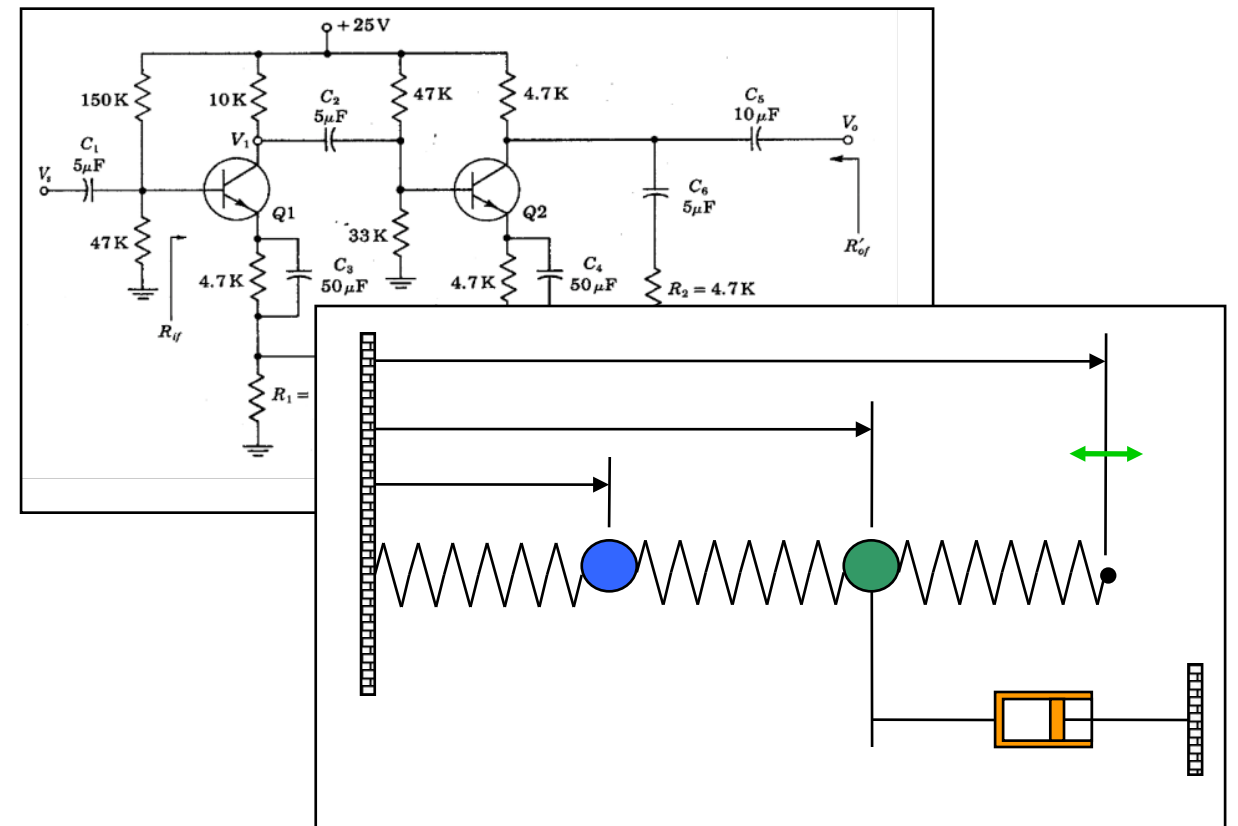
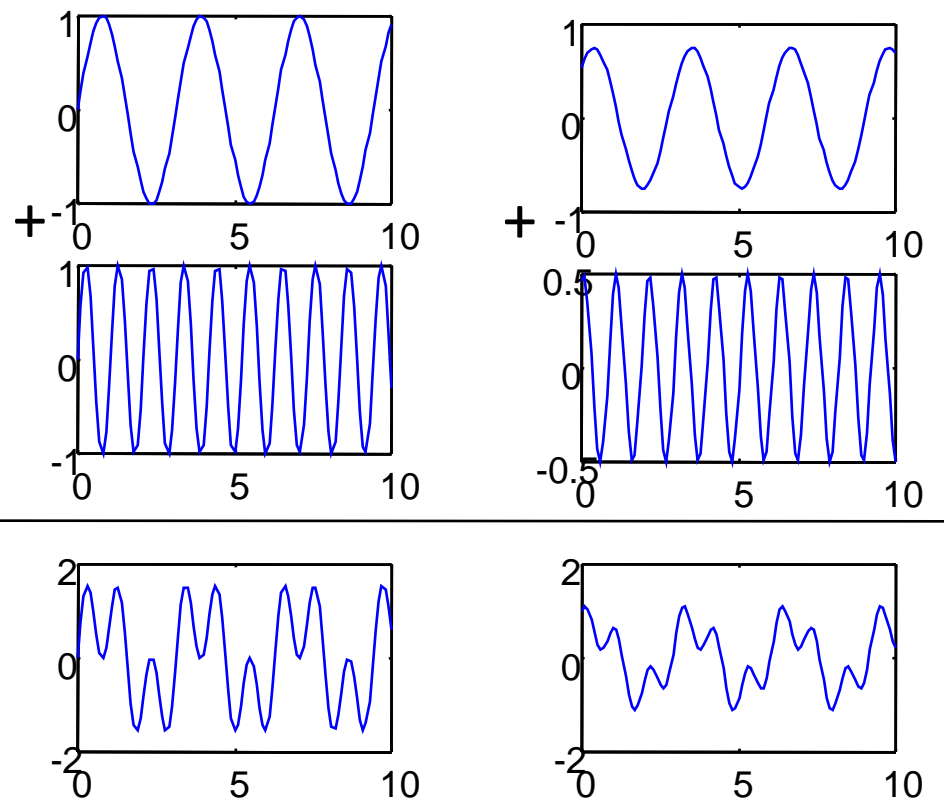
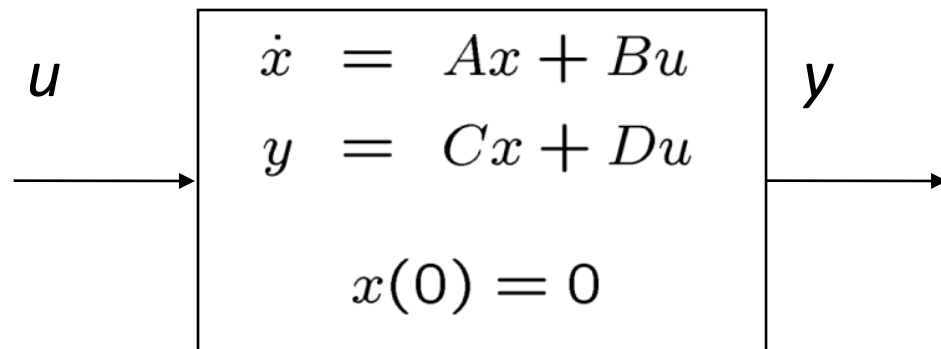
$$v_{1,2} = \begin{bmatrix} 1 \\ 1 \\ \pm 1i \\ \pm 1i \end{bmatrix} \quad v_{3,4} = \begin{bmatrix} 1 \\ -1 \\ \pm \sqrt{2}i \\ \mp \sqrt{2}i \end{bmatrix}$$

Eigenvalues of A:

- For zero damping, $j\omega_1$ and $j\omega_2$
- ω_1 and ω_2 correspond frequency response peaks
- The eigenvectors for these eigenvalues give the *mode shape*:
 - In-phase motion for lower freq.
 - Out-of phase motion for higher freq.



Summary: Linear Systems



- Properties of linear systems
 - Linearity with respect to initial condition and inputs
 - Stability characterized by eigenvalues
 - Many applications and tools available
 - Provide local description for nonlinear systems

$$y(t) = Ce^{At}x(0) + \int_{\tau=0}^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

Linearization Around an Equilibrium Point

$$\begin{array}{l} \dot{x} = f(x, u) \\ y = h(x, u) \end{array} \longrightarrow \begin{array}{l} \dot{z} = Az + Bv \\ w = Cz + Dv \end{array}$$

“Linearize” around $x=x_e$

$$f(x_e, u_e) = 0 \quad y_e = h(x_e, u_e)$$

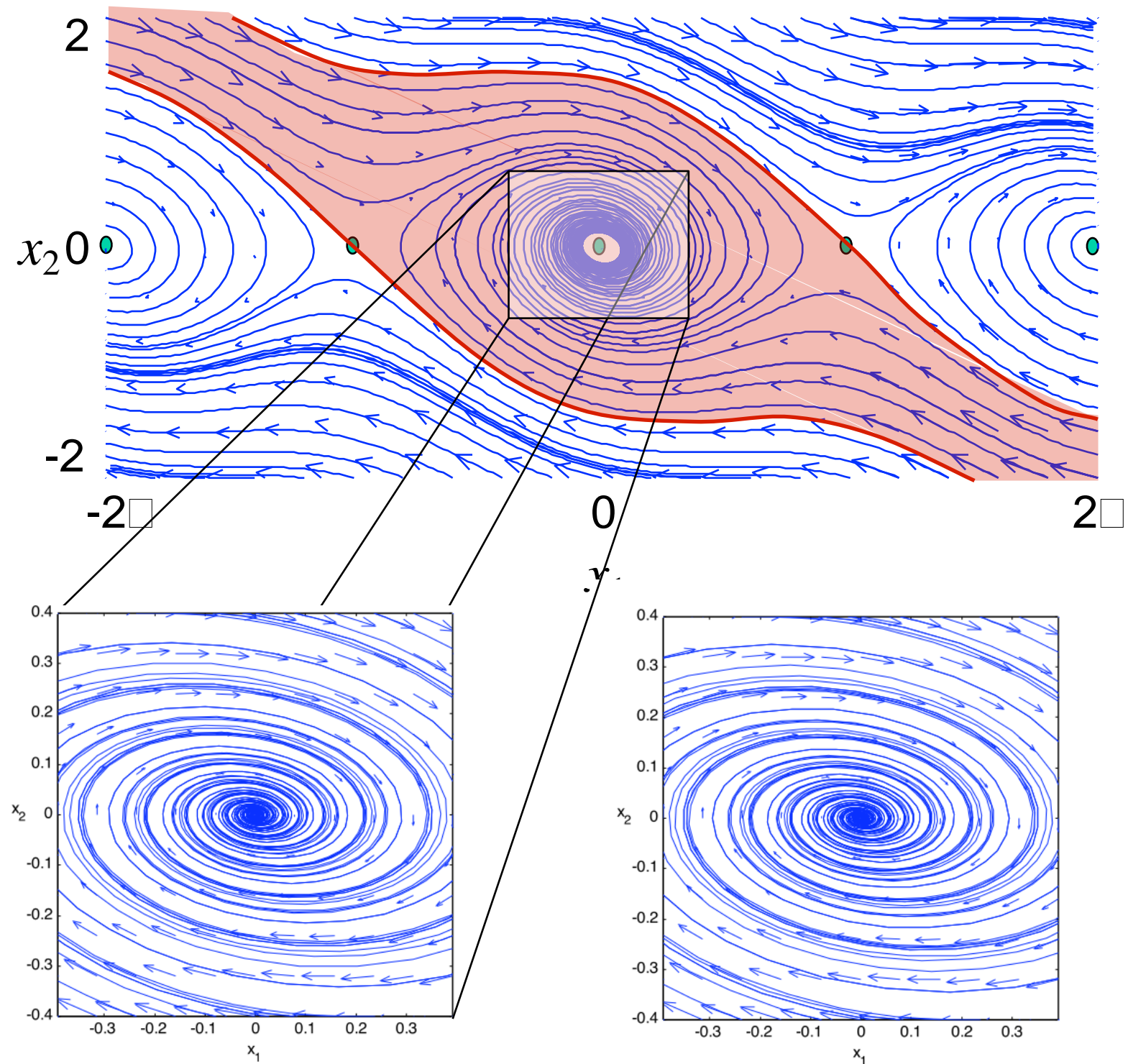
$$z = x - x_e \quad v = u - u_e \quad w = y - y_e$$

$$A = \left. \frac{\partial f}{\partial x} \right|_{(x_e, u_e)} \quad B = \left. \frac{\partial f}{\partial u} \right|_{(x_e, u_e)}$$

$$C = \left. \frac{\partial h}{\partial x} \right|_{(x_e, u_e)} \quad D = \left. \frac{\partial h}{\partial u} \right|_{(x_e, u_e)}$$

Remarks

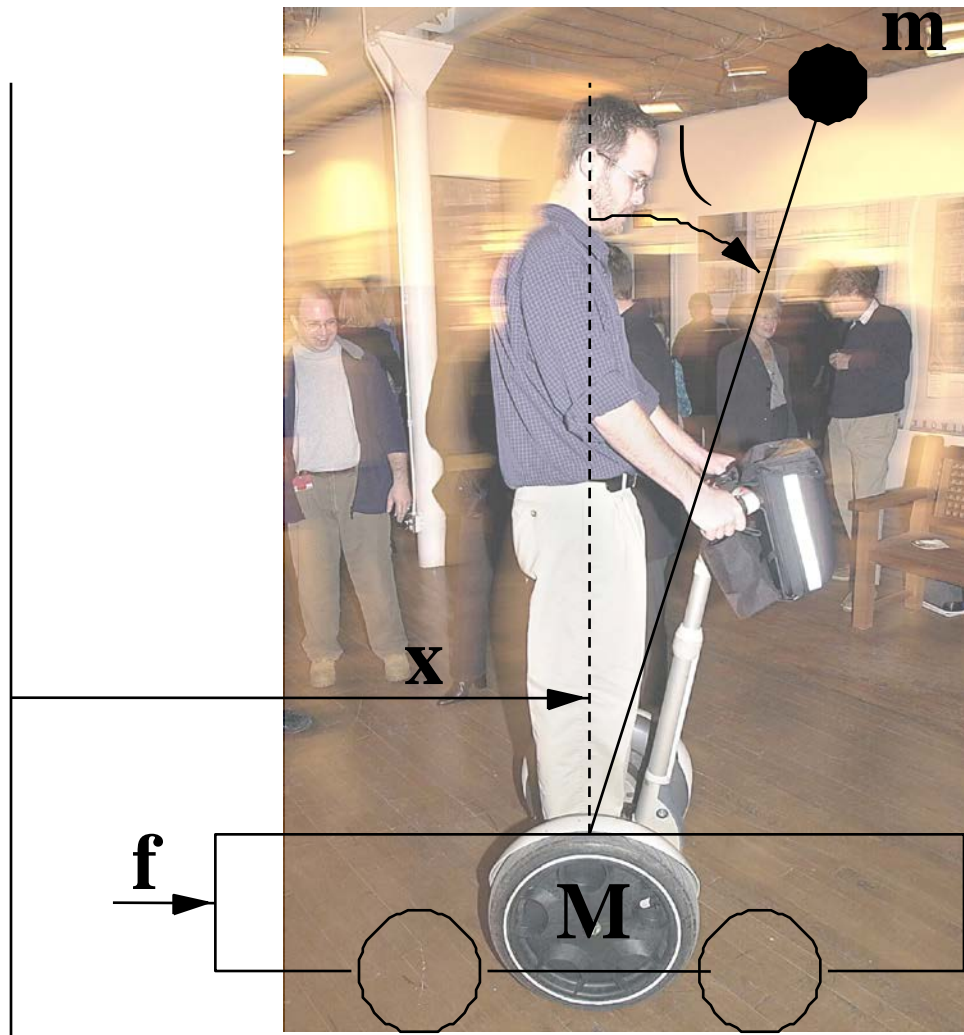
- In examples, this is often equivalent to small angle approximations, etc
- Only works *near* to equilibrium point



Full nonlinear model

Linear model (honest!)

Example: Inverted Pendulum on a Cart



$$(M + m)\ddot{x} + ml \cos \theta \ddot{\theta} = -b\dot{x} + ml \sin \theta \dot{\theta}^2 + f$$

$$(J + ml^2)\ddot{\theta} + ml \cos \theta \ddot{x} = -mgl \sin \theta$$

- State: $x, \theta, \dot{x}, \dot{\theta}$
- Input: $u = F$
- Output: $y = x$
- Linearize according to previous formula around $\theta = 0$

$$\frac{d}{dt} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & \frac{m^2 g l^2}{J(M + m) + M m l^2} & \frac{-(J + m l^2) b}{J(M + m) + M m l^2} & 0 \\ 0 & \frac{m g l (M + m)}{J(M + m) + M m l^2} & \frac{-m l b}{J(M + m) + M m l^2} & 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \frac{J + m l^2}{J(M + m) + M m l^2} \\ \frac{m l}{J(M + m) + M m l^2} \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix}$$