

# Métodos de Energia

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**Ref. e ilustrações : An Introduction to the Mechanics of Solids . Crandall et. All. – 2.6, 5.8, 6.8, 7.8**

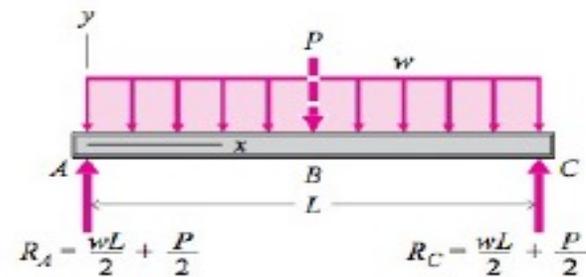


Figure 8-30

### Example Problem 8-19

Determine the deflection at the center of a simply supported beam of constant cross section and span  $L$  carrying a uniformly distributed load  $w$  over its entire length.

#### SOLUTION

The deflection is required at a point where there is no unique point load. Thus, a dummy load  $P$  is introduced at the center of the beam in the direction of the desired deflection. In the free-body diagram of Fig. 8-30, the dashed force  $P$  represents the dummy load. The moment equation is

$$M_r = M_w + M_P = \frac{wLx}{2} - \frac{wx^2}{2} + \frac{Px}{2} - P \left\langle x - \frac{L}{2} \right\rangle^1$$

where the quantity  $\langle x - L/2 \rangle^1$  is zero for all  $x \leq L/2$  (see Section 8-5). The partial derivative of  $M_r$  with respect to  $P$  is

$$\frac{\partial M_r}{\partial P} = \frac{x}{2} - \left\langle x - \frac{L}{2} \right\rangle^1$$

The dummy force  $P$  is equated to zero after the partial derivative is taken, and the deflection is given by

$$\begin{aligned} EIv &= \int_0^L M_r \frac{\partial M_r}{\partial P} dx \\ &= \int_0^L \left( \frac{wLx}{2} - \frac{wx^2}{2} \right) \left( \frac{x}{2} - \left\langle x - \frac{L}{2} \right\rangle^1 \right) dx \end{aligned}$$

which, for ease of integration, can be written as

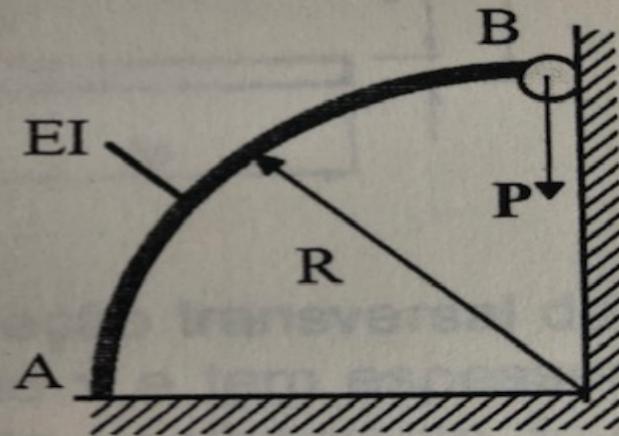
$$EIv = \frac{w}{4} \int_0^L (Lx^2 - x^3)dx + \frac{w}{4} \int_{L/2}^L (L^2x - 3Lx^2 + 2x^3)dx = \frac{5wL^4}{384}$$

Since the deflection is positive, it is in the direction of the force,

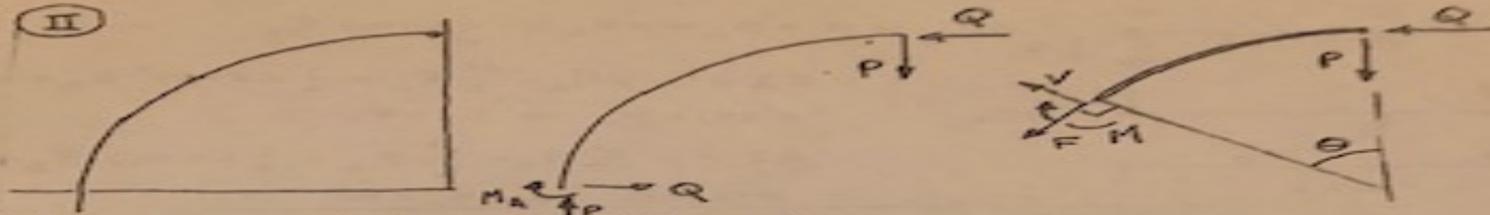
$$v = \frac{5wL^4}{384EI} \downarrow \quad \text{Ans.}$$

This result corresponds to case 7 of Table B-19 (Appendix B).

(9) Calcular o deslocamento



(II)



i) 
$$F(\theta) = -P \sin \theta - Q \cos \theta$$

$$V(\theta) = P \cos \theta - Q \sin \theta$$

$$M(\theta) = -PR \sin \theta + QR(1 - \cos \theta)$$

ii) 
$$U = \frac{1}{2} \int_0^{\pi/2} \frac{R^3}{EI} [-P \sin \theta + Q(1 - \cos \theta)]^2 d\theta +$$

$$+ \frac{1}{2} \int_0^{\pi/2} \frac{R}{EA} (P \sin \theta + Q \cos \theta)^2 d\theta$$

$$\int_0^{\pi/2} \sin^2 \theta d\theta = \int_0^{\pi/2} \cos^2 \theta d\theta = \frac{\pi}{4} ; \int_0^{\pi/2} \sin \theta \cos \theta d\theta = \frac{1}{2} ;$$

$$\int_0^{\pi/2} \sin \theta d\theta = \int_0^{\pi/2} \cos \theta d\theta = 1 \quad \therefore$$

$$U = \frac{1}{2} \frac{R^3}{EI} \left[ \frac{\pi}{2} Q^2 + \frac{\pi}{4} (P^2 + Q^2) - 2PQ - 2Q^2 + \frac{1}{2} 2PQ \right] +$$

$$+ \frac{1}{2} \frac{R}{EA} \left[ \frac{\pi}{4} (P^2 + Q^2) + \frac{1}{2} 2PQ \right]$$

$$U = \frac{R^3}{2EI} \left[ \frac{\pi}{4} (P^2 + 3Q^2) - PQ - 2Q^2 \right] + \frac{R}{2EA} \left[ \frac{\pi}{4} (P^2 + Q^2) + PQ \right]$$

flexão ( $U_M$ )

compressão ( $U_F$ )

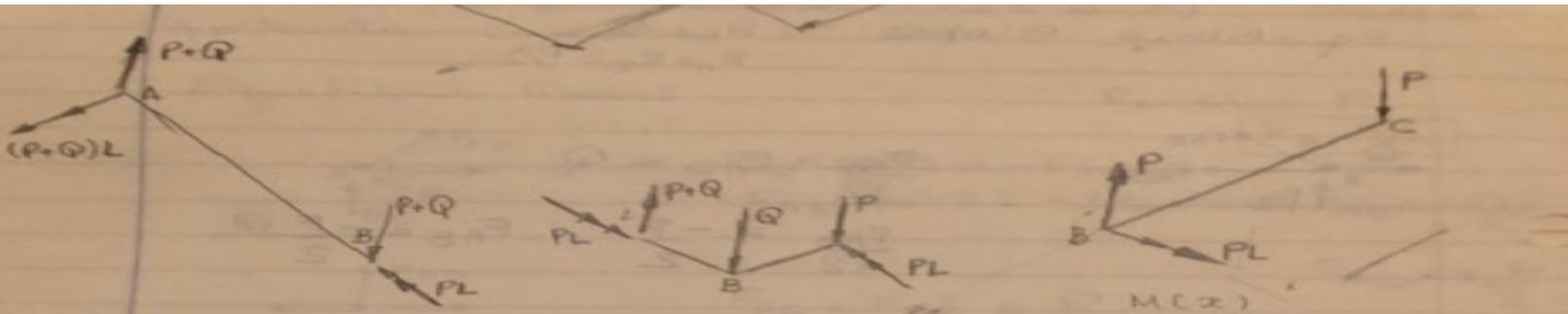
iii) 
$$\delta_H = 0 \Rightarrow \frac{\partial U_M}{\partial Q} = 0 \Rightarrow \frac{3\pi Q}{2} - P - 4Q = 0 \Rightarrow$$

$$Q = \frac{2P}{3\pi - 8} = 1.404 P$$

$$\delta_V = \frac{\partial U_M}{\partial P} = \frac{R^3}{2EI} \left( \frac{\pi P}{2} + Q \right)$$

$$\delta_V = \frac{R^3 P}{EI} \left( \frac{\pi}{4} + \frac{1}{3\pi - 8} \right) = 0.0835 \frac{R^3 P}{EI}$$





Calcular o deslocamento em C e B e

$$U = U_{AB} + U_{BC}$$

$$U_{AB} = \underbrace{\int_0^L \frac{(P+Q)^2 x^2}{2EI_z} dx}_{\text{flexão}} + \underbrace{\int_0^L \frac{PL^2}{2GI_x} dx}_{\text{torção}} + \dots$$

termos de  
de cortante  
desprezíveis em  
relação aos de

$$U_{BC} = \int_0^L \frac{P(L-z)^2}{2EI} dz$$

$$v_B = \frac{\partial U}{\partial Q} = \int_0^L \frac{(P+Q)x^2}{EI_z} dx = \frac{(P+Q)L^3}{3EI_z}$$

$$v_C = \frac{\partial U}{\partial P} = \int_0^L \frac{(P+Q)x^2}{EI_z} dx + \int_0^L \frac{PL^2}{GI_x} dx + \int_0^L \frac{P(L-z)^2}{EI_z} dz$$

$$v_c = \underbrace{\frac{(P+Q)L^3}{3EI_z}}_{\text{flexão de AB } (\psi_1)} + \underbrace{\frac{PL^3}{GI_x}}_{\text{torção de AB } (\psi_2)} + \underbrace{\frac{PL^3}{3EI_z}}_{\text{flexão de BC } (\psi_3)}$$

Para cada...

Exemplo 5.1 do Crandall..